



**OPERATING AND SERVICE MANUAL**

**MODEL 1111A**

**SERIAL PREFIXED: 422-**

**AC CURRENT AMPLIFIER**

**CENTRAL ENGINEERING  
INSTRUMENT POOL**

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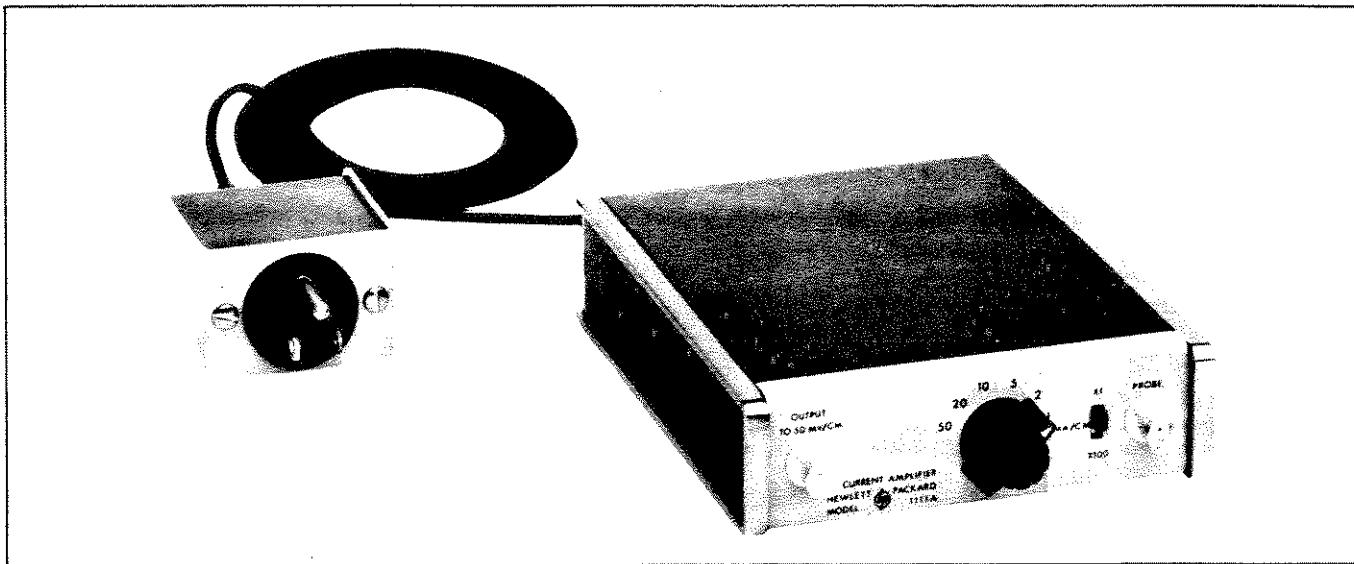


Figure 1-1. Model 1111A AC Current Amplifier

Table 1-1. Specifications for Model 1111A with Model 1110A Probe

<b>SENSITIVITY:</b> 1 ma/cm to 50 ma/cm in X1  100 ma/cm to 5 amps/cm in X100, 1, 2, 5 sequence for X1 or X100	<b>MAXIMUM AC CURRENT:</b> Above 700 cps: 50 amps pk-pk Below 700 cps: decreases at 1.4 amps/20 cps
<b>ACCURACY:</b> ±3% on X1 sensitivity  ±4% on X100 sensitivity	<b>OUTPUT IMPEDANCE:</b> 50 ohms
<b>BANDWIDTH:</b> 50 cps to 20 Mc	<b>DIMENSIONS:</b> 1-1/2 in. high, 5-1/8 in. wide, 6 in. deep
<b>RISE TIME:</b> 18 nsec	<b>WEIGHT:</b> Approximately 2 lb
<b>NOISE:</b> Less than 100 $\mu$ a pk-pk, referred to input	<b>POWER:</b> 115 or 230 volts ±10%, 50 to 1000 cps, 1.5 watts

## SECTION I

### GENERAL INFORMATION

#### **1-1. DESCRIPTION AND APPLICATIONS.**

1-2. The Hewlett-Packard Model 1111A AC Current Amplifier, shown in Figure 1-1, is a stable, wide-band amplifier to be used with the  $\Phi$  Model 1110A Probe. The Model 1111A amplifies the Probe output, extends the low frequency response to 50 cps, and provides 12 ranges of sensitivity from 1 ma/cm to 5 amps/cm (used with 50 mv/cm sensitivity oscilloscope). Complete specifications are given in Table 1-1.

1-3. The Model 1111A is designed for use with an oscilloscope which has a calibrated vertical amplifier with 50 mv/cm sensitivity. When used with this sensitivity oscilloscope, the Model 1111A's attenuator may be read directly in milliamperes per centimeter

deflection on the CRT. The Model 1111A may be used with an oscilloscope having different sensitivity, but the conversion ratio must then be used.

#### **1-4. INSTRUMENT IDENTIFICATION.**

1-5. The Hewlett-Packard Company uses a two-section, eight-digit serial number to identify instruments (e.g. 000-00000). The serial number is located on a plate attached to the instrument rear panel. The first three digits are a serial prefix number, also appearing on the title page of this manual, and the last five digits identify a specific instrument. If the first three digits of the instrument serial number are not the same as those appearing on the title page, change sheets included with the manual will define differences between other instruments and the Model 1111A described herein. If the change sheets are missing, your  $\Phi$  Field Engineer can supply the information.

## SECTION II

### PREPARATION FOR USE

#### **2-1. INCOMING QUALITY CONTROL INSPECTION.**

2-2. MECHANICAL INSPECTION. Upon receipt of your Model 1111A, check that the contents are intact and as ordered. Inspect the instrument for any damage incurred in shipping. If the instrument is damaged, notify the carrier immediately (refer to the warranty which appears on the inside back cover of this manual).

2-3. PERFORMANCE CHECK. Check the performance of the Model 1111A by making the tests as outlined in Paragraph 5-4 of this manual. This check may be used to verify instrument specifications and as part of an incoming quality control inspection.

#### **2-4. AC POWER CONSIDERATION.**

##### **2-5. POWER REQUIREMENTS.**

2-6. The Model 1111A requires an AC power source of 115 or 230 volts  $\pm 10\%$ , single phase, 50 to 1000 cps. The power required is approximately 1.5 watts. The Model 1111A is normally shipped from the factory for use from a 115-volt power source. To convert the instrument for use from a 230-volt source, slide the 115-230 switch to the "230" position. This switch is located on the power plug assembly.

##### **2-7. THREE-CONDUCTOR CONNECTOR.**

2-8. To protect operating personnel the National Electrical Manufacturers Association (NEMA) recommends that the instrument panel and cabinet be

grounded. This instrument is equipped with a three-pin power plug which, when plugged into an appropriate receptacle, grounds the instrument. The offset round pin on the plug is the ground connection. To retain the protection feature when operating the instrument from a two-contact outlet, use a three-conductor to two-conductor adapter and connect the adapter wire to ground.

#### **2-9. RACK INSTALLATION.**

2-10. The Model 1111A may be placed in a  $\Phi$  1051A combining case which may then be installed in an instrument rack. The Combining Case may also be mounted in the rack space of a  $\Phi$  Model 1117A Testmobile for convenience of keeping related-use instruments together (the  $\Phi$  1051A also adapts 1/3 width modular instruments to a rack).

#### **2-11. REPACKAGING FOR SHIPMENT.**

2-12. The following is a general guide for packaging an instrument for shipment. If there are any questions regarding packaging methods, contact your Hewlett-Packard Field Office.

- a. Wrap the instrument in heavy paper or plastic before placing it in the shipping container.

- b. Use plenty of packing material around all sides of the instrument and protect surfaces with cardboard strips.
- c. Place the instrument in a heavy cardboard carton or wooden box. Seal the container with heavy tape or metal straps.
- d. Mark the packing container "FRAGILE-DELICATE INSTRUMENT".

2-13. If an instrument is being returned to Hewlett-Packard Company for servicing or repair, attach a tag to the instrument specifying owner, desired action, model number, and serial number. Ship the instrument to Hewlett-Packard Customer Service at the address on the warranty page. All correspondence should refer to an instrument by model number and the full (eight-digit) serial number.

## SECTION III

### OPERATING INSTRUCTIONS

#### **3-1. INTRODUCTION.**

3-2. The Model 1111A provides amplification of the output of the Model 1110A Probe, and calibrated control of the sensitivity. Front-panel controls set the sensitivity in milliamperes/centimeter when used with an oscilloscope with 50 mv/cm sensitivity.

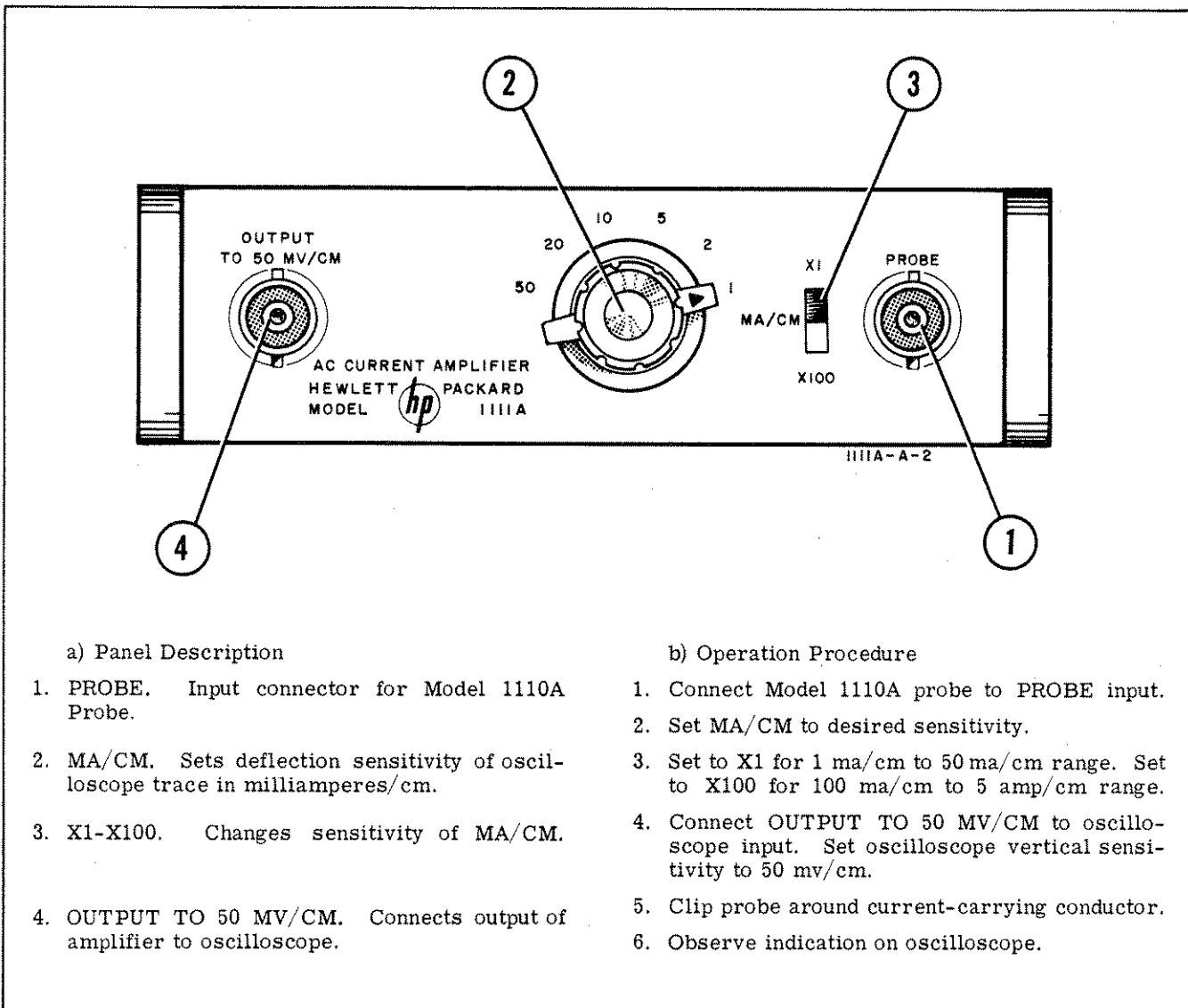
#### **3-3. PANEL DESCRIPTION AND OPERATING PROCEDURE.**

3-4. Figure 3-1(a) provides a brief description of front panel controls and connectors, keyed by number to the panel illustration. A step-by-step operating procedure is provided in Figure 3-1(b). Additional operating considerations are given in Paragraph 3-5.

#### **3-5. OPERATING CONSIDERATIONS.**

3-6. GENERAL. The following paragraphs contain information about making measurements using the Model 1111A with the Model 1110A Current Probe. While most of the considerations relate to the Model 1110A, the information is provided here since the two instruments are designed for use together.

3-7. DIRECTION OF CURRENT FLOW. The arrow on the probe body indicates the direction of conventional current flow which produces a positive output from the probe and amplifier. Thus there is a "sense of polarity" when observing current waveforms on the



##### a) Panel Description

1. PROBE. Input connector for Model 1110A Probe.
2. MA/CM. Sets deflection sensitivity of oscilloscope trace in milliamperes/cm.
3. X1-X100. Changes sensitivity of MA/CM.
4. OUTPUT TO 50 MV/CM. Connects output of amplifier to oscilloscope.

##### b) Operation Procedure

1. Connect Model 1110A probe to PROBE input.
2. Set MA/CM to desired sensitivity.
3. Set to X1 for 1 ma/cm to 50 ma/cm range. Set to X100 for 100 ma/cm to 5 amp/cm range.
4. Connect OUTPUT TO 50 MV/CM to oscilloscope input. Set oscilloscope vertical sensitivity to 50 mv/cm.
5. Clip probe around current-carrying conductor.
6. Observe indication on oscilloscope.

Figure 3-1. Front Panel Description and Operation Procedure

oscilloscope, and the polarity can be reversed by removing the probe from any wire, rotating the probe 180°, and clipping it around the wire again.

**3-8. INCREASING SENSITIVITY.** The sensitivity of the probe may be increased by looping the wire through two or more times. The increase in sensitivity is directly proportional to the number of loops; i.e., 2 loops = twice sensitivity. However, the increase in sensitivity is accompanied by an increase in the series loading effect due to the probe, which increases as the square of the number of loops. Also, the looped wire itself adds inductance and shunt capacitance to ground which may be significant at high frequencies.

**3-9. SUMMING CURRENTS.** The probe may be clipped around wires carrying different currents as well as around loops of the same wire. In either case the instantaneous output of the probe is the algebraic sum of the instantaneous currents through the probe. In this way currents may be balanced (in push-pull circuits, for example) by clipping the probe around two wires in which the currents are 180° out of phase as they pass through the probe, and adjusting the circuit for minimum output from the probe.

**3-10. EFFECTS OF EXTERNAL FIELDS.** The probe is magnetically shielded to minimize the effects of external magnetic fields. However, strong fields near power transformers or electric motors may cause an unwanted output from the probe and amplifier. To check for such fields, hold the probe with jaws closed and no wire through it in the region in which you intend to make the measurement. If the probe output is excessive compared to the expected measurement, make the measurement at some other point along the wire farther from the source of the field, or orient the probe lead for minimum undesired output. If there is little or no output from the probe and amplifier the field will not affect the measurement.

**3-11. PEAK CURRENT.** The maximum peak-to-peak current which the probe and amplifier will accept is a function of frequency. Figure 3-2 shows a plot of peak-to-peak current vs frequency.

**3-12. MAXIMUM DC CURRENT.** The Current Amplifier and Probe will perform as specified in Table 1-1 if the DC current present is less than 0.5 amperes. Above 0.5 amperes DC, performance is derated since the DC current acts to decrease Probe head inductance and to raise the low frequency -3 db point.

**3-13. HIGH FREQUENCY RESPONSE.** Performance of Current Amplifier and Probe will be within specifications if the load capacitance presented to the output of the Model 1111A is less than 30 pf. The high frequency -3 db point is determined by the capacitive load at the input. The typical high frequency oscilloscope has an input capacitance of 28 pf, hence high frequency operation of the Probe and Amplifier is not affected.

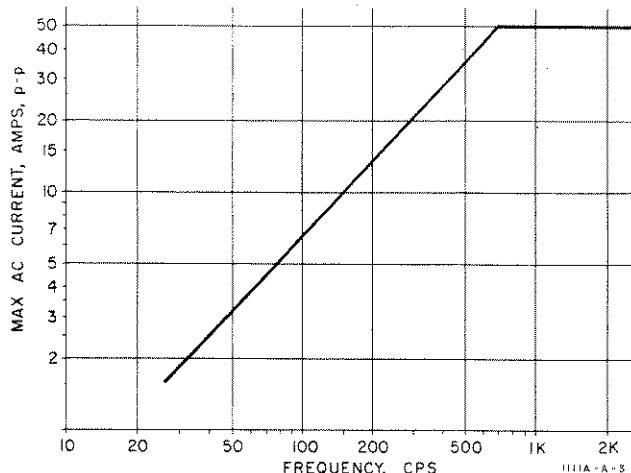


Figure 3-2. Peak-to-Peak Current vs Frequency

**3-14. AMPLIFIER GAIN.** The gain of interest for the Model 1111A is a transresistance, or output millivolts per milliampere of current at the input, which is the dimension of ohms ( $mv/ma = \text{ohms}$ ). Since the input impedance varies somewhat with range and frequency (see Paragraph 3-15), this does not correspond to a stable voltage gain  $E_{\text{out}}/E_{\text{in}}$ . For convenience in using the Model 1111A amplifier in other applications, Table 3-1 lists gains for all sensitivity ranges.

**3-15. INPUT IMPEDANCE.** The X100 range is a constant 0.5 ohms ( $\pm 3\%$ ) in series with an inductance of about  $30 \times 10^{-9} \text{ H}$  (about 2" of wire). In the X1 position, input impedance is more complex, but up to about 100 kc can be approximated by a 2000 microfarad capacitor in series with a resistance of between 0.2 and 0.5 ohms, depending on sensitivity setting. At higher frequencies, the input impedance becomes dependent on feedback factor changes with frequency.

Table 3-1. Amplifier Gain

Range	$MV_{\text{out}}/MA_{\text{in}}$ (1111A only)	$MV_{\text{out}}/MA_{\text{in}}$ (with probe)
1	5000	50
2	2500	25
5	1000	10
10	500	5
20	250	2
50	100	1
Switching to X100 attenuates all ranges 100 times.		

## SECTION IV

### PRINCIPLES OF OPERATION

#### **4-1. INTRODUCTION.**

4-2. The Model 1111A is a current amplifier which is specifically designed for use with the Model 1110A Current Probe. As described in the following paragraphs, the Model 1111A consists of an input amplifier, an output amplifier, and a power supply. Refer to the instrument schematic, Figure 5-9, for circuit references.

#### **4-3. INPUT AMPLIFIER.**

4-4. To obtain the maximum low-frequency potential of the probe, as well as optimum linearity and large-signal performance, the probe should have a load impedance which is much lower than the winding resistance of the current transformer in the probe. The input amplifier provides such a load, and also accomplishes the current-to-voltage conversion necessary for oscilloscope display. Circuit operation is described in Paragraph 4-5, and the biasing arrangement is described in Paragraph 4-10.

#### **4-5. CIRCUIT OPERATION.**

4-6. The input amplifier consists of a grounded-base amplifier Q1 and cascode amplifier Q2/Q3. The cascode amplifier combination, using two transistors, gives a lower effective collector-base capacitance than that of one transistor. The simplified schematic in Figure 4-1 shows the conditions for the 1 MA/CM range, and omits a bias-setting adjustment (R14) at the base of Q3.

4-7. An ac signal current from the probe is split between Q1 emitter (impedance of about 15 ohms to ground) and R20 (about 2000 ohms). However, due to the unity current gain of grounded-base amplifier Q1, any portion of the input signal current flowing into Q1 emitter is applied directly to Q2 base, causing about 100 times as much current to flow through R20. Therefore, because of this feedback, about 99% of the input signal current flows through R20, and only 1% into Q1 emitter. This action has two results: 1) since only 1% of the signal current flows into the 15-ohm emitter impedance of Q1, the input voltage developed is only 1% of what this current would develop in a 15-ohm resistor, meaning that the input impedance is reduced by a factor of 100, down to .15 ohm; 2) since 99% of input signal current ( $i_S$ ) flows through R20, and because the input emitter is very close to ground potential, the output from Q3 is a voltage equal to  $(.99i_S)(R20)$ , which is almost independent of transistor parameters. If current gain of the cascode amplifier were to drop to 50 (a 2:1 change) then 98% of the input signal current would flow through R20, and gain would change only 1%.

4-8. Capacitor C6 is used for high-frequency gain stabilization by introducing a local negative feedback loop around the cascode amplifier. This capacitor reduces the total effect of transistors Q2 and Q3 and all their stray capacitances to that of a single -6 db/octave gain slope at high frequencies. The gain-crossover frequency (at which gain = 1) of the cascode amplifier is adjusted by varying this capacitance. The proper setting is determined on the basis of optimum

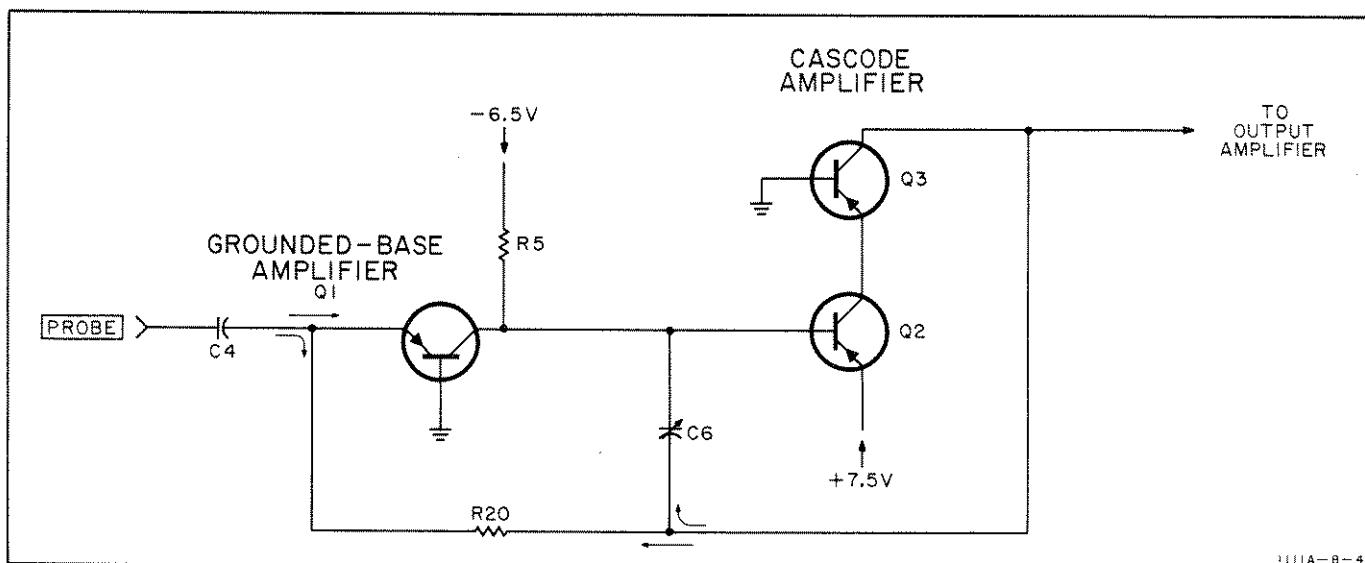


Figure 4-1. Simplified Input Amplifier Schematic

overall transient response (overshoot and rise time). Pulse Rounding Adjust R14 varies the collector voltage of the lower half of the cascode amplifier, altering the high-frequency response of the local feedback loop. Adjustment is made for optimum pulse response.

4-9. Sensitivity range is changed by switching in other values of feedback resistance (R20 in Figure 4-1). Since about 99% of input signal current flows in the feedback resistor, the gain function  $\frac{E_{out}}{i_s}$  is approximately numerically equal to the feedback resistor in ohms. As the resistor is changed to smaller values, more bias current is required to provide adequate maximum output voltage. For this reason, R6 and R7 are switched in to reduce the Q1 collector load.

#### 4-10. DC BIASING.

4-11. The dc voltages and currents are set as follows: the base of Q2 operates at about +7.0 volts (constant 0.5 volt base-emitter drop from +7.5 volt supply). Due to the 10-volt drop across breakdown diode CR7, the collector of Q1 must run at -3.0 volts, 10 volts negative from +7 volts. Since Q1 collector is at -3 volts, R5 has -6.5 volts at one end and -3 volts at the other, and so has 3.5 volts across it. This causes a current of 3.5/2400, or 1.4 ma to flow in R5. The 1.4 ma dc current flows 99% through Q1 collector and 1% through Q2 base, due to the current gain of 100 in the cascode amplifier and gain of unity in Q1. (About .0138 ma in Q2 base causes about 1.38 ma in Q3 collector, which then flows through R20 and Q1, and joins with the .0138 ma base current to make the 1.4 ma in R20). Thus for a given set of dc voltages, R5 sets the current in all three transistors, and R20 affects only the dc voltage at the cascode amplifier output, which must be between +7 volts and ground for proper operation of the cascode stage.

4-12. Resistor R11 is switched in on the two most sensitive ranges to augment the bias current in Q2.

#### 4-13. OUTPUT AMPLIFIER.

4-14. Following the input amplifier is a voltage divider, emitter follower, and straight common-emitter output amplifier, in that order. The voltage divider is used to reduce the gain for the 20 MA/CM and 50 MA/CM ranges (rather than further reduction of feedback resistance in the input amplifier). The output stage emitter resistor, R34, is unbypassed except for R35 and C19, which are switched in to compensate frequency response on the 1 and 2 MA/CM ranges against stray capacitances. Calibration is set by R40, which forms a current divider with R41. Output impedance is 50 ohms, so the Model 1111A will drive any length of 50-ohm cable with flat response, independent of termination.

#### 4-15. POWER SUPPLY.

4-16. The supplies, although labelled +7.5 and -6.5, are actually generated by one floating 14 volt regulated supply. The split to +7.5 and -6.5 is done by Q4 and Q5 in the final amplifier. The total 14 volt supply is tapped by R32 and R38, which places the base of Q4 approximately centered on the supply. Transistors Q4 and Q5 then act as dc emitter followers to solidly place ground at 7.5 volts from the positive end of the supply, and 6.5 volts from the negative end.

4-17. Resistor R33 (200 ohms) is really the emitter resistor for Q5, and sets the dc current in Q5, but has no effect on the voltage split between the positive and negative supplies.

4-18. When the interstage attenuator is switched in (on 20 and 50 MA/CM ranges), current from the +7.5 volt supply (through Q3 collector) would flow to ground through R29 (201 ohms) or R28 (50 ohms), subtracting from the available collector current of Q5. To obviate this, R8 (1200 ohms) is switched in, which passes this current directly to the -6.5 volt supply, rebalancing the load on the positive and negative supplies. Output transistor thus still gets all the bias current established by R33.

## SECTION V

### MAINTENANCE

#### **5-1. TEST EQUIPMENT REQUIRED.**

5-2. INSTRUMENTS. Table 5-1 lists the test instruments required for the performance checks and for making the Model 1111A adjustments. Substitute equipment should provide performance according to the specifications listed in Table 5-1. Be sure test equipment has been recently calibrated and always allow manufacturer's suggested warmup period to obtain full accuracy.

5-3. SPECIAL LOADS. Three special loads are required:  $50\ \Omega$ ,  $600\ \Omega$ , and  $22\text{ pf}$ . These may be made by using the appropriate connector-adapter and component required. Figure 5-1 illustrates the  $600\ \Omega$  load required. The  $50\ \Omega$  load may be made using a  $50 \pm 0.5\ \Omega$  resistor and either the dual banana plug

connector or a BNC-banana plug adapter. For the capacitive load, use a  $22\text{ pf}$  capacitor ( $\text{hp}$  Stock No. 0140-0145) and a BNC connector ( $\text{hp}$  Stock No. 1250-0079). Solder the capacitor between center conductor (on rear of connector) and the shield (next to threaded section).

#### **5-4. PERFORMANCE CHECK.**

5-5. The procedure of Paragraphs 5-6 through 5-9 should determine if the Model 1111A is operating within its specifications. If performance is out of specifications, refer to Paragraphs 5-10 through 5-13 for the adjustment procedure or to the troubleshooting suggestions of Paragraph 5-14. In the procedures using the Model 1110A Probe, always be sure the head surfaces are clean and that the jaws close firmly.

Table 5-1. Test Equipment Required

No.	Description	Important Specifications	Use	Recommended Equipment
1	Signal Generator	Output: 1 volt into $50\ \Omega$ , constant with frequency Frequency: 50 Kc-20 Mc	Check sensitivity, accuracy and bandwidth	$\text{hp}$ Model 606A
2	AC Voltmeter	Accuracy: 1% Range: 0.1 volts	Check sensitivity accuracy and bandwidth	$\text{hp}$ Model 400H
3	Current Probe	Bandwidth: 45 Mc Rise Time: 8 nsec Output: 1 mv/ma	Check sensitivity, accuracy and bandwidth Adjust pulse response	$\text{hp}$ Model 1110A
4	Audio Oscillator	Range: 50 cps - 50 Kc Output: 1.5 volts into $600\ \Omega$ constant with frequency	Check bandwidth Adjust gain	$\text{hp}$ Model 200CD
5	R.F. Millivoltmeter	Range: 0.1 volts Bandwidth: 1 Mc - 20 Mc Accuracy: $\pm 3\%$ full scale	Check bandwidth	$\text{hp}$ Model 411A
6	Sampling Oscilloscope and plug-in	Bandwidth: 100 Mc Sync Pulse: 1.5 volts into $50\ \Omega$ , 1.5 nsec risetime Sensitivity: 10 mv/cm	Adjust pulse response	$\text{hp}$ Model 185B and Model 187B
7	High Frequency Oscilloscope and plug-in	Bandwidth: 50 Mc Sensitivity: .05 v/cm	Check noise	$\text{hp}$ Model 175A and Model 1751A
8	Square Wave Generator	Frequency: 400 Kc Rise Time: 3 nsec Output: 0.5 volts into $50\ \Omega$	Adjust pulse and high frequency response	Tektronix Model 107 Square Wave Generator
9	Special Loads	$50\ \Omega$ : $50 \pm 0.5\ \Omega$ Resistor $600\ \Omega$ : See Figure 5-1 $22\text{ PF}$ : Capacitor and BNC connector	See Paragraph 5-3	

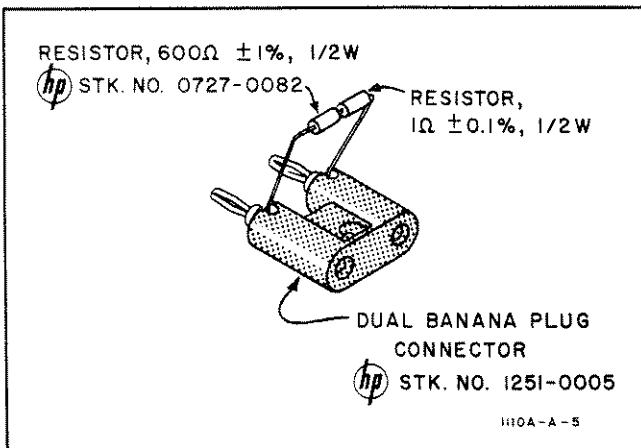


Figure 5-1. Special 600  $\Omega$  Load

#### 5-6. SENSITIVITY AND ACCURACY.

- a. Refer to Table 5-1 and Figure 5-2 and connect test equipment. Items required are 2, 3, 4 and 9.
- b. Set Voltmeter range to 0.1 volts.
- c. Set Oscillator frequency to 50 kc.
- d. Disconnect Voltmeter from Model 1111A output and reconnect Voltmeter across the 600  $\Omega$  load.
- e. Set Oscillator output for a Voltmeter reading of 0.1 volts.
- f. Disconnect the Voltmeter from the load and reconnect it to the Model 1111A output.
- g. Set the Model 1111A sensitivity to 1 MA/CM, X1.
- h. Check Model 1111A output according to Table 5-2.
- i. Disconnect Voltmeter from Model 1111A output and reconnect it across the 600  $\Omega$  load.
- j. Set the Oscillator output for a Voltmeter reading of 1.0 volts.
- k. Disconnect the Voltmeter from the 600  $\Omega$  load and connect it to the Model 1111A output.
- l. Set the Model 1111A sensitivity to 1 MA/CM, X100.
- m. The Voltmeter reading should be 0.01 volts  $\pm 4\%$ .

#### 5-7. NOISE.

- a. Connect the Probe (item 3 in Table 5-1) to the Model 1111A input.

b. Connect the Model 1111A output to the Oscilloscope plug-in (item 7 in Table 5-1).

c. Set oscilloscope and plug-in SENSITIVITY to .05 VOLTS/CM, SWEEP TIME to 50  $\mu$ SEC/CM, SWEEP MODE to PRESET, and TRIGGER SOURCE to LINE.

d. Set Model 1111A sensitivity to 1 MA/CM, X1.

e. Position the Probe and Amplifier (no input to probe) so the external field coupling is minimum as viewed on CRT.

f. With oscilloscope trace intensity set for normal, look closely at the high frequency random noise displayed. Any noise should be less than 1 mm peak-to-peak, which corresponds to less than 100  $\mu$ A p-p.

#### 5-8. BANDWIDTH.

- a. Refer to Table 5-1 and Figure 5-2 and connect test equipment. Items required are 2, 3, 4 and 9.
- b. Set Model 1111A sensitivity to 1 MA/CM, X1.
- c. Set Voltmeter range to 0.1 volts.
- d. Set Oscillator frequency to 10 Kc and amplitude for a zero db reading on the Voltmeter.
- e. Set Oscillator frequency to 50 cps.
- f. Voltmeter reading should be -3 db or greater.

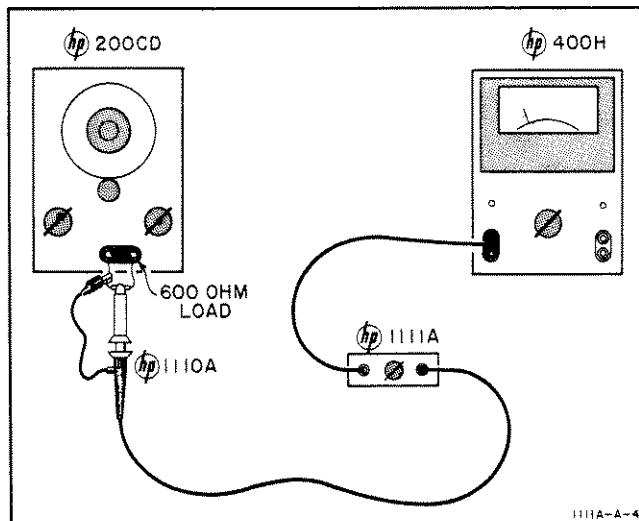


Figure 5-2. Oscillator-Voltmeter Test Setup

Table 5-2. Sensitivity and Accuracy Check

Model 1111A Sensitivity, MA/CM	Voltmeter Range, Volts	Voltmeter Reading, Volts
1	.1	0.1 $\pm 3\%$
2	.1	0.05 $\pm 3\%$
5	.03	0.02 $\pm 3\%$
10	.01	0.01 $\pm 3\%$
20	.01	0.005 $\pm 3\%$
50	.003	0.002 $\pm 3\%$

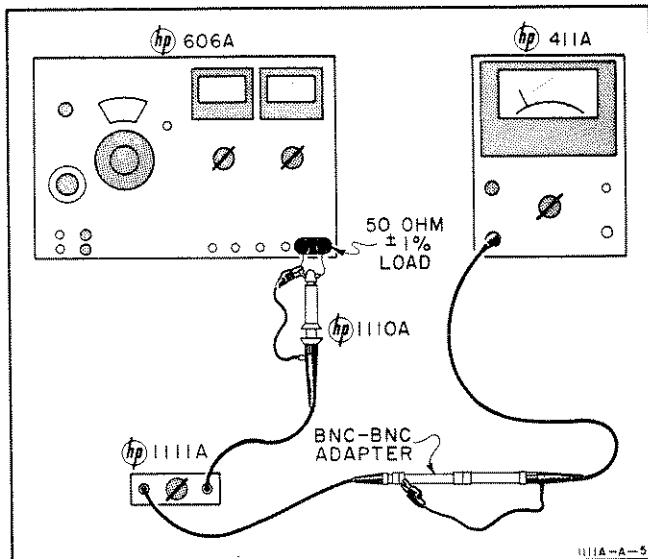


Figure 5-3. Signal Generator - RF Millivoltmeter Test Setup

g. Repeat procedure starting with step b, using appropriate Voltmeter range, and checking other Model 1111A sensitivity ranges.

h. Disconnect test setup. Refer to Figure 5-3 and Table 5-1 and connect test equipment specified, using items 1, 3, 5 and 9.

i. Set Model 1111A sensitivity to 1 MA/CM, X1.  
j. Set the Millivoltmeter range to 0.1 volts.

k. Set the Signal Generator frequency to 1 Mc and the output amplitude for a zero db reading on the Millivoltmeter.

m. Set the Signal Generator frequency to 20 Mc.

n. Millivoltmeter reading should be -3 db or greater.

p. Repeat procedure starting with step j, using appropriate Millivoltmeter range, and checking the other Model 1111A sensitivity ranges.

#### 5-9. RISE TIME.

a. Refer to Table 5-1 and Figure 5-4 and connect specified equipment, items 3 6, and 9. The  $50 \Omega$  load is connected to the oscilloscope sync pulse output.

b. Set Oscilloscope MODE to FREE RUN and switch on SYNC PULSE.

c. Set Model 1111A sensitivity to 1 MA/CM, X1.

d. Adjust Oscilloscope and plug-in SENSITIVITY, TIME SCALE and MAGNIFIER controls to display leading edge of pulse.

e. The rise time (between 10% and 90% amplitude points) should be 18 nanoseconds or less.

f. Check other Model 1111A sensitivity ranges for the same rise time specification.

#### 5-10. ADJUSTMENTS.

##### 5-11. AMPLIFIER GAIN SET.

- Refer to Table 5-1 and Figure 5-2 and connect specified equipment, items 2, 3, 4 and 9.
- Set Oscillator frequency to 50 Kc.
- Set Model 1111A sensitivity to 1 MA/CM, X1.
- Disconnect Voltmeter from Model 1111A output and reconnect Voltmeter across Oscillator output.
- Set Oscillator output for reading of 0.1 volts.
- Reconnect Voltmeter to Model 1111A output.
- Adjust R40 for Voltmeter reading of 0.1 volts.
- Refer to Table 5-2 to check the Model 1111A output on other sensitivity settings.

##### 5-12. PULSE AND HIGH FREQUENCY RESPONSE.

5-13. The adjustments for pulse and high frequency response will have some interaction, requiring a repeat of the procedure to optimize the performance. When an adjustment affects more than one sensitivity range, a compromise setting may be necessary. The objective for these adjustments is to obtain the best pulse response combination possible; this means best rise time within specifications with least ringing and overshoot.

a. Refer to Table 5-1 and Figure 5-5, and connect specified equipment, items 3, 6, 7, and 8. One additional item is required: a capacitive load, described in Paragraph 5-3. Use a BNC tee connector to connect the capacitive load and oscilloscope probe to the Model 1111A output.

b. Set the Square Wave Generator amplitude control fully clockwise (output approximately 0.5 volts) and frequency control to about 400 kc.

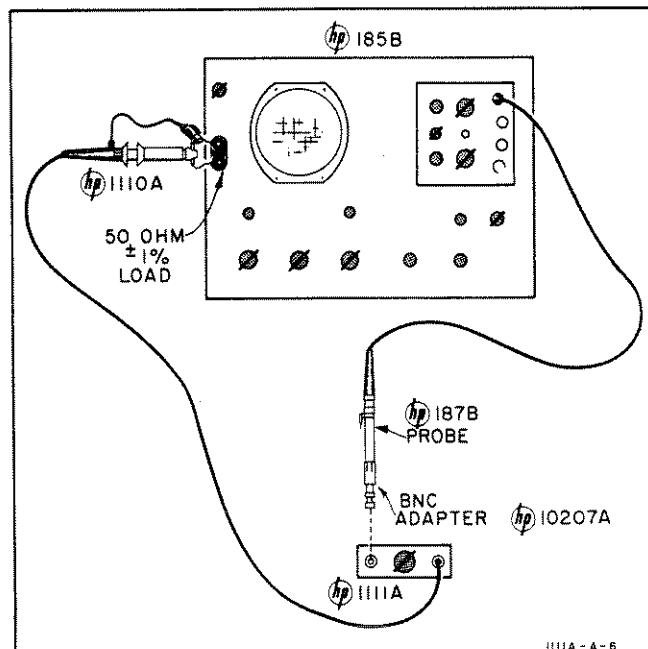


Figure 5-4. Rise Time Check Setup

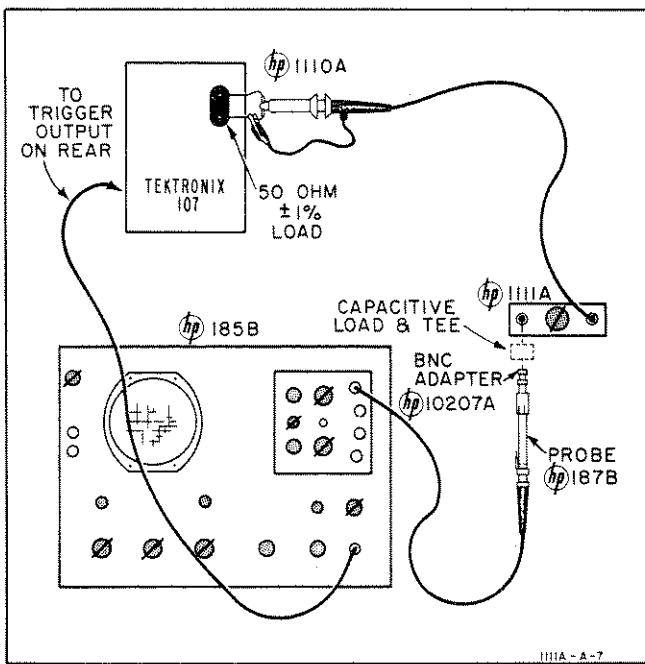


Figure 5-5. Pulse and High Frequency Response Test Setup

- c. Set Model 1111A sensitivity to 1 MA/CM, X1.
- d. Set Oscilloscope and plug-in controls as follows: TIME SCALE to 200 NSEC/CM, TIME SCALE MAGNIFIER to X2, TRIGGER SLOPE to -, SENSITIVITY to 200 MILLIVOLTS/CM, and SCANNING control to INTERNAL.
- e. Adjust controls to obtain a good display of the positive pulse.
- f. Set Pulse Rounding Adjust R14 for best leading edge on square wave.
- g. Adjust C6 for best leading edge.
- h. Set sensitivity control to 2 MA/CM, X1.
- i. Adjust C13 for best leading edge.
- j. Set sensitivity control to 5 MA/CM, X1.
- k. Adjust C12 for best leading edge.
- m. Set sensitivity to 10 MA/CM, X1.
- n. Adjust C11 for best leading edge.
- p. Check pulse response on all ranges, and make compromise readjustments if necessary.

#### 5-14. TROUBLESHOOTING.

##### 5-15. CIRCUIT VOLTAGES.

5-16. The schematic diagram, Figure 5-9, gives typical dc voltages and ac waveforms for troubleshooting. Conditions of measurement are listed on page 5-8.

##### 5-17. NO OPERATION.

- a. Check ac power.
- b. Be sure X100 attenuator has not inadvertently been switched in.
- c. Check Model 1110A probe separately.
- d. Measure +7.5 and -6.5 volt supplies. If correct proceed to step e; if not proceed to step g.
- e. Check bias voltages within the amplifiers. If biases are considerably off in the input amplifier, check Q1, Q2, Q3, and CR7. Also check for proper switch contacting. If trouble persists, proceed to step f.
- f. If all biases are right, clip the probe on a sinusoidal current of about 60 ma, 50 kc. Set sensitivity to 10 MA/CM, X1. Then trace the signal, using a 10:1 scope probe, from Q3 collector through Q4 and Q5 to the output. (Signal voltages within the input amplifier are small and not significant for troubleshooting. If biases are right, and C4 is good, the input amplifier should work.)
- g. If the +7.5 or -6.5 volt supplies are in error, measure total voltage from -6.5 to +7.5 volts with a floating (ungrounded) dc voltmeter. This voltage should be 14 volts  $\pm 1$  volt, and it should not change visibly from 102 to 128 volt ac line voltage. If above 15 volts dc check regulator transistor Q6 and breakdown diode CR10. If below 13 volts, proceed to step h. If between 13 and 15 volts, power supply is operating correctly; proceed to step j.

h. Check unregulated dc voltage across C1 (black and white wires) with a floating (ungrounded) dc voltmeter. At 115 volts ac line, this should read approximately 20 to 30 volts dc. If low, check current through R47 with a dc milliammeter. The current should be about 37 to 50 ma. If above 50 ma, proceed to step k. If below 37 ma, with low unregulated voltage, check transformer, rectifiers, and power cable. If the unregulated voltage is above 35 volts dc, proceed to step i.

i. Check dc current into Q6 emitter. Current should be about 36 ma to 48 ma. If low, and 14 volt supply is still low (from step g), supply regulator is at fault. If high, the load has excessive drain, which must be corrected before the supply will regulate properly. Check filter and bypass capacitors for shorts, and test amplifier transistors.

j. If 14 volt measurement is correct (step g) but -6.5 or +7.5 voltages are wrong, check amplifier transistors Q5 and Q5, then Q3 and Q2. Then check filter and bypass capacitors for shorts.

k. If unregulated voltage is low and current through R47 is high, measure Q6 emitter current, which should be 36 to 48 ma. If emitter current is high, load (amplifier or filter capacitors) is shorted. If low, Q6 or CR10 may be shorted.

##### 5-18. EXCESSIVE SQUARE-WAVE SAG.

- a. Check low-frequency response of Model 1110A probe against its specifications. Clean probe jaw mating surfaces with a pencil eraser for perfect contact.

b. Make sure the input impedance of the oscilloscope used with the Model 1111A is about 100K ohms, or sag will result from the output coupling capacitor (0.1 microfarads) in the Model 1111A.

c. If sag persists, clip a 10:1 scope probe on Test Point 1, with the current probe clipped on a square wave peak-to-peak current of approximately 10 times the MC/CM of the range in use. If sag appears here, replace C4. Check power supply capacitors.

d. If sag does not exist at Test Point 1, trace the signal through the resistive divider (on switch), through C18, Q4, and Q5. Check C20 in Q5 collector circuit, and center pin of J2.

#### 5-19. EXCESSIVE SQUARE-WAVE OVERSHOOT.

5-20. This is very unlikely except in cases of transistor replacement. In any case, be sure the trouble is not in the test set-up. See adjustment procedure for calibration method. If excessive overshoot actually is present, carry out the pulse response adjustment procedure fully, for all ranges.

#### 5-21. OUT OF CALIBRATION.

5-22. Use the calibration procedure to be sure the trouble is really due to the Model 1111A. Small variations can be adjusted with R40, but any large discrepancy may be due to a faulty probe, or some amplifier or power supply problem. A check of dc voltages should locate the faulty components.

### **5-23. REPAIR AND REPLACEMENT.**

#### 5-24. COMPONENT LOCATION.

5-25. Figure 5-6, 5-7, and 5-8 identify all the components of the Model 1111A which have reference designators. These components, and those miscellaneous parts having no designators, are listed in Section VI with replacement stock information.

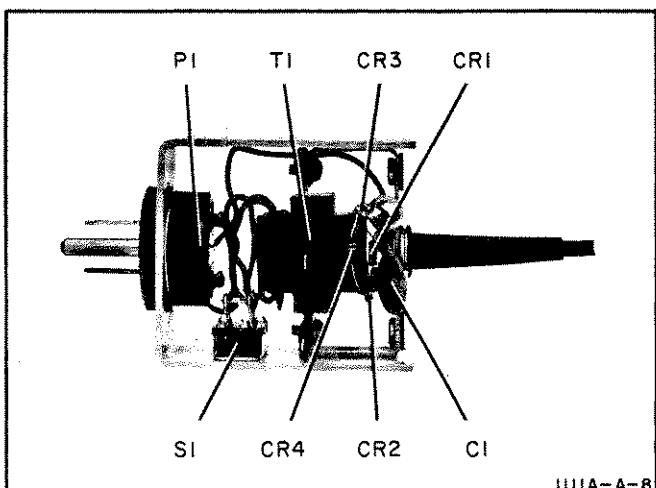


Figure 5-6. Power Supply Assembly

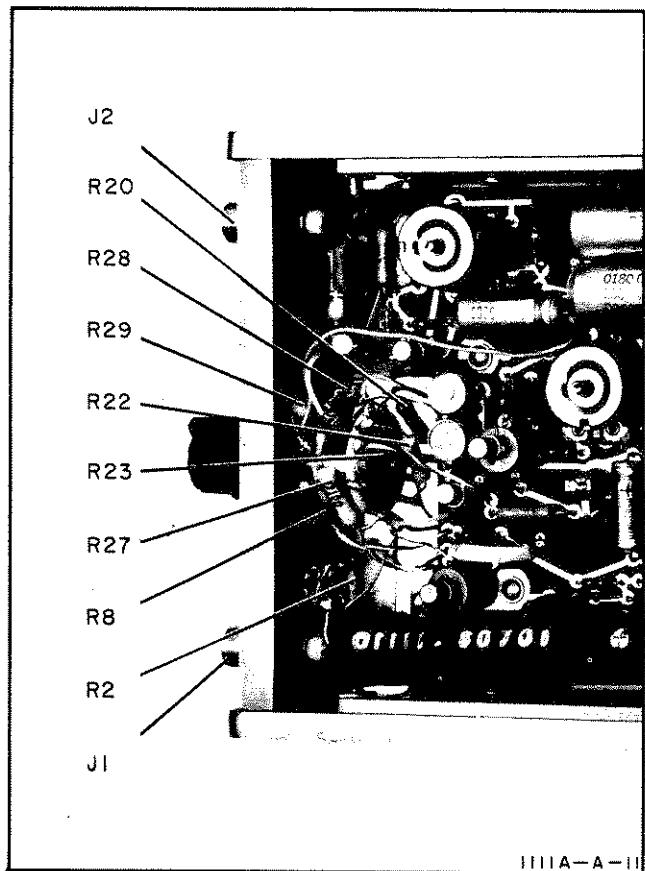


Figure 5-7. Front Panel and Sensitivity Switch Components

#### 5-26. REPLACING ETCHED CIRCUIT BOARD COMPONENTS.

5-27. The etched circuit board, assembly A101, has components on one side of the board and the etched circuit conducting paths on the opposite side. The connection between sides of the board is completed by a plated conductive layer of metal through component holes. Hewlett-Packard Service Note M-20D also contains useful information on etched circuit repair. The important steps and considerations are:

a. Use a low heat (37 to 47.5 watts, less than 800° F idling temperature), slightly bent chisel tip (1/16 to 1/8 inch diameter) soldering iron, and a small diameter, high tin content solder. If a rosin solder is used, clean the area thoroughly after soldering.

b. Components may be removed by placing the soldering iron on the component lead on either side of the board, and pulling up on the lead. If heat is applied to the component side of the board, greater care is required to avoid damage to the component (especially true for diodes). If heat damage may occur, grip the lead with a pair of pliers to provide a heat sink between the soldering iron and component.

c. If a component is obviously damaged or faulty, clip the leads close to the component and then unsolder the leads from the board.

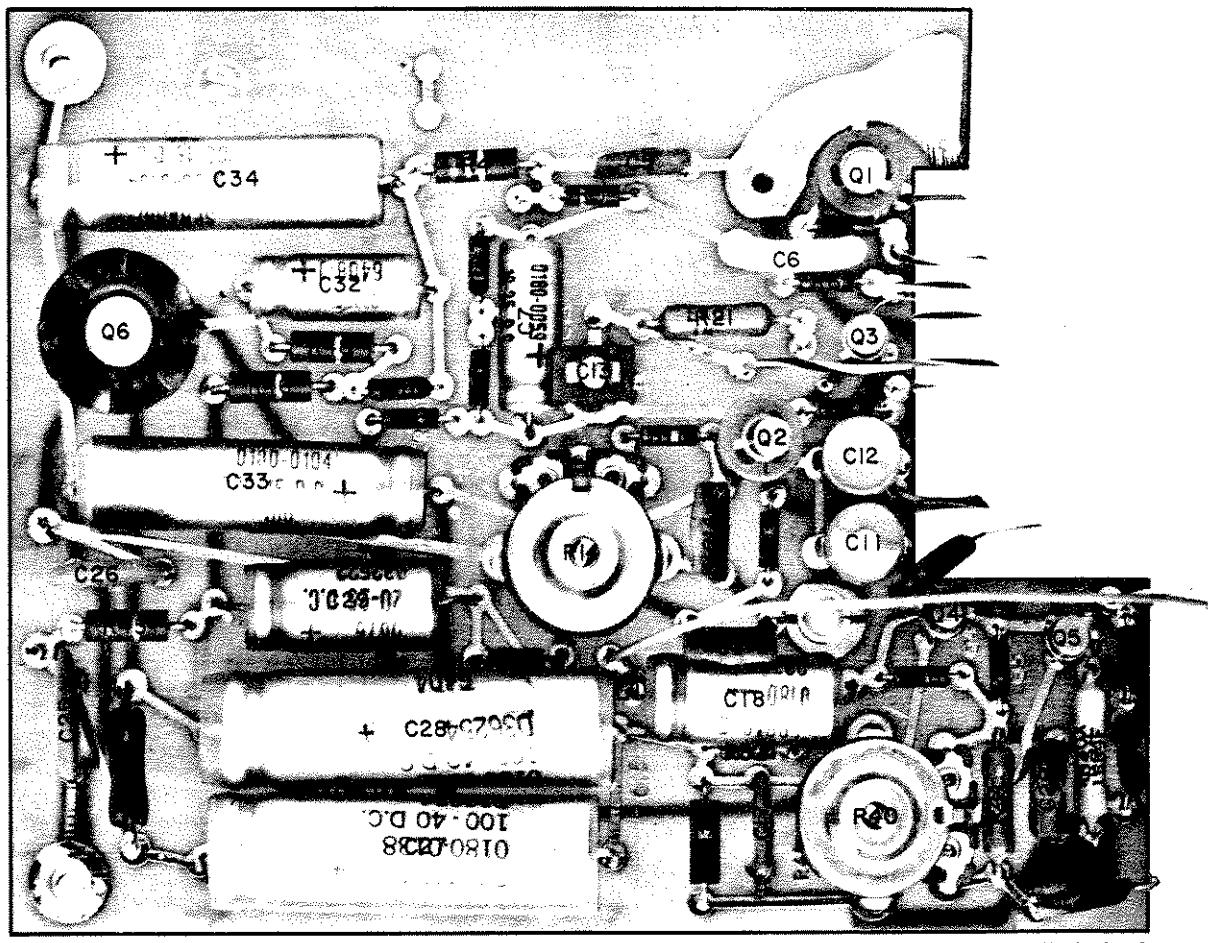
d. Large components such as potentiometers and tube sockets may be removed by rotating the soldering iron from lead to lead and applying steady pressure to lift the part free (the alternative is to clip the leads of a damaged part).

e. Since the conductor part of the etched circuit board is a metal plated surface, covered with solder, use care to avoid overheating and lifting the conductor from the board. A conductor may be cemented back

in place with a quick drying acetate base cement (use sparingly) having good insulating properties. Another method for repair is to solder a section of good conducting wire along the damaged area.

f. Clear the solder from the circuit board hole before inserting a new component lead. Heat the solder in the hole, remove the iron, and quickly insert a pointed non-metallic object, such as a toothpick.

g. Shape the new component leads and clip to proper length. Insert the leads in the holes and apply heat and solder, preferably on the conductor side.



1111A-A-12

Figure 5-8. Etched Circuit Board Components

Table 5-3. Calibration and Component Replacement Record  
For Hewlett-Packard Company Model 1111A Current Amplifier

Instrument Serial No. \_\_\_\_\_

## CALIBRATION

## COMPONENT REPLACEMENT

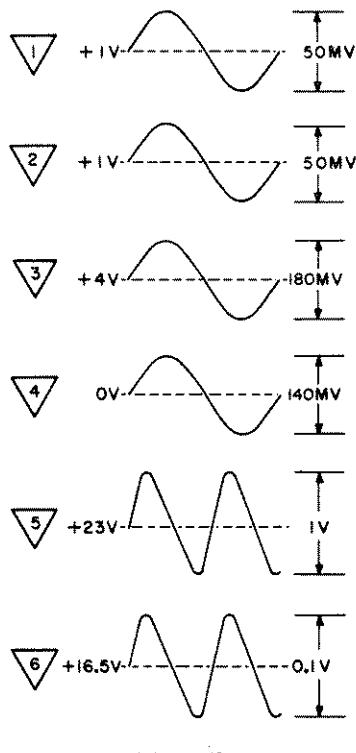
## CONDITIONS OF MEASUREMENT

DC Measurements

Sensitivity set to: 10 MA/CM, X1.

Waveform Measurements

- a. Sensitivity set to: 10 MA/CM, X1.
- b. For Test Points 1 through 4, clip current probe around wire carrying sinusoidal current of 60 ma, 50 kc.
- c. No input signal for Test Points 5 and 6.



1111A-A-13

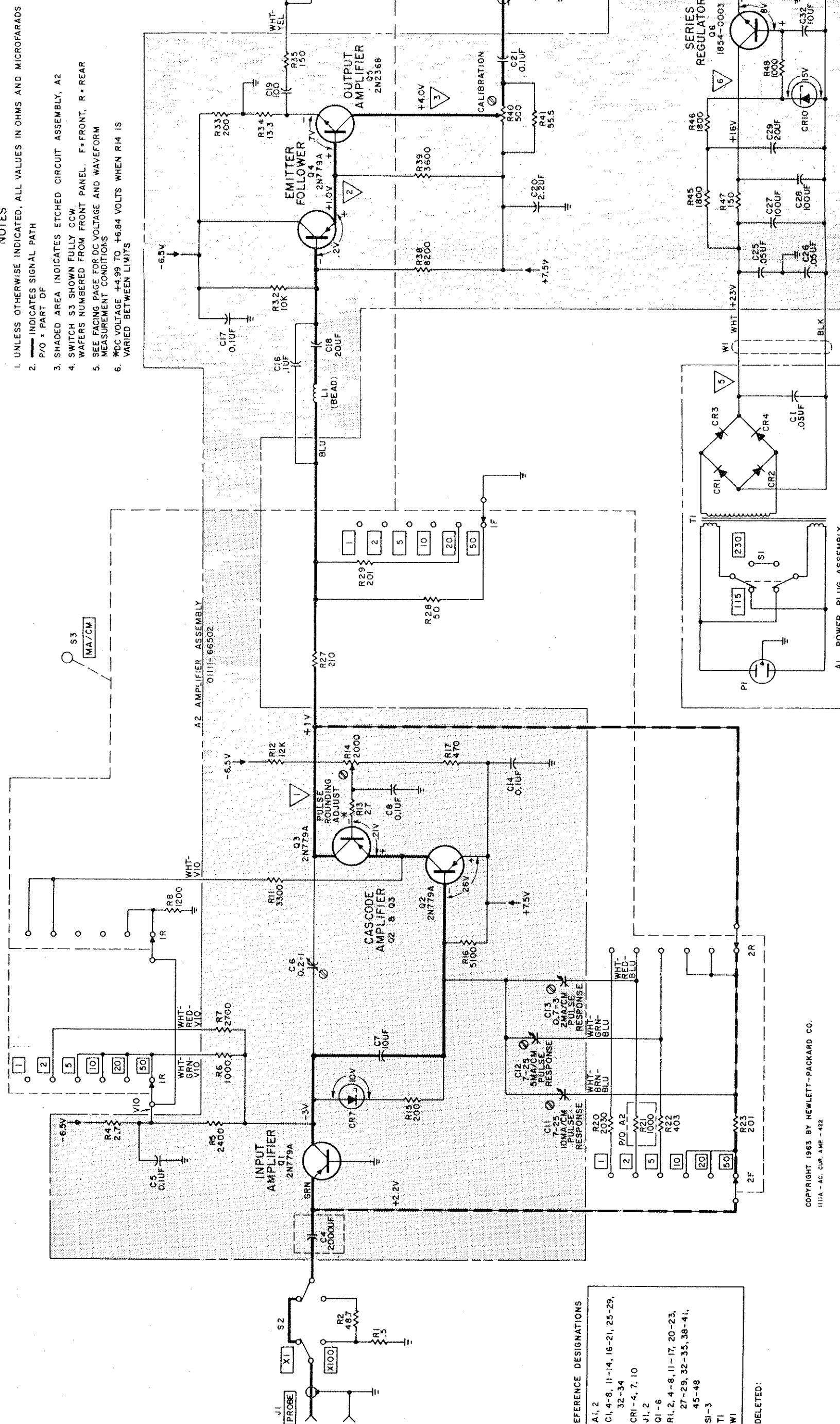


Figure 5-9. AC Current Amplifier Schematic

## SECTION VI

### REPLACEABLE PARTS

#### 6-1. INTRODUCTION.

6-2. This section contains information for ordering replacement parts. Table 6-1 lists parts in alphabetical order of their reference designators and indicates the description and stock number of each part, together with any applicable notes. Table 6-2 lists parts in alpha-numerical order of their stock numbers and provides the following information on each part:

- a. Description of the part (see list of abbreviations below).
- b. Typical manufacturer of the part in a five-digit code; see list of manufacturers in appendix.
- c. Manufacturer's stock number.
- d. Total quantity used in the instrument (TQ column).
- e. Recommended spare part quantity for complete maintenance during one year of isolated service (RS column).

6-3. Miscellaneous and cabinet parts not indexed by reference designators are listed at the end of Table 6-1.

#### 6-4. ORDERING INFORMATION.

6-5. To order a replacement part, address order or inquiry either to your nearest Hewlett-Packard field office or to

CUSTOMER SERVICE  
Hewlett-Packard Company  
395 Page Mill Road  
Palo Alto, California

or, in Western Europe, to

Hewlett-Packard S.A.  
54 Route des Acacias  
Geneva, Switzerland

6-6. Specify the following information for each part:

- a. Model and complete serial number of instrument.
- b. Hewlett-Packard stock number.
- c. Circuit reference designator.
- d. Description.

6-7. To order a part not listed in Tables 6-1 and 6-2, give a complete description of the part and include its function and location.

#### REFERENCE DESIGNATORS

A	= assembly
B	= motor
C	= capacitor
CR	= diode
DL	= delay line
DS	= device signaling (lamp)
E	= misc electronic part

F	= fuse
FL	= filter
J	= jack
K	= relay
L	= inductor
M	= meter
MP	= mechanical part

P	= plug
Q	= transistor
R	= resistor
RT	= thermistor
S	= switch
T	= transformer

V	= vacuum tube, neon bulb, photocell, etc.
W	= cable
X	= socket
Y	= crystal
Z	= network

#### ABBREVIATIONS

A	= amperes	F	= farads	NC	= normally closed	S-B	= slow-blow
BP	= bandpass	FXD	= fixed	NE	= neon	SE	= selenium
BWO	= backward wave oscillator	GE	= germanium	NO	= normally open	SECT	= section(s)
CER	= ceramic	GL	= glass	NPO	= negative positive zero (zero temperature coefficient)	SI	= silicon
CMO	= cabinet mount only	GRD	= ground(ed)	NSR	= not separately replaceable	SIL	= silver
COEF	= coefficient	H	= henries	OBD	= order by description	SL	= slide
COM	= common	HG	= mercury	OX	= oxide	SPL	= special
COMP	= composition	HR	= hour(s)	P	= peak	TA	= tantalum
CONN	= connection	IMPG	= impregnated	PC	= printed circuit board	TD	= time delay
CRT	= cathode-ray tube	INCD	= incandescent	PF	= picofarads = $10^{-12}$ farads	TI	= titanium dioxide
DEPC	= deposited carbon	INS	= insulation(ed)	PP	= peak-to-peak	TOG	= toggle
EIA	= Tubes or transistors meeting Electronic Industries' Association standards will normally result in instrument operating within specifications; tubes and transistors selected for best performance will be supplied if ordered by stock numbers.	K	= kilo = 1000	PIV	= peak inverse voltage	TOL	= tolerance
7		LIN	= linear taper	POR	= porcelain	TRIM	= trimmer
01194		LOG	= logarithmic taper	POS	= position(s)	TWT	= traveling wave tube
7		MEG	= meg = $10^6$	POLY	= polystyrene	U	= micro = $10^{-6}$
01		M	= milli = $10^{-3}$	POT	= potentiometer	VAC	= vacuum
7		MINAT	= miniature	RECT	= rectifier	VAR	= variable
01		METFLM	= metal film	ROT	= rotary	W/	= with
7		MFR	= manufacturer	RMS	= root-mean-square	W	= watts
01		MOM	= momentary	RMO	= rack mount only	WW	= wirewound
7		MTG	= mounting			W/O	= without
01		MY	= mylar			*	= optimum value selected at factory, average value shown (part may be omitted)

Table 6-1. Reference Designation Index

Reference Designation	Stock No.	Description #	Note
A1	01111-67601	POWER PLUG ASSEMBLY	
A2	01111-66502	AMPLIFIER ASSEMBLY	
A3	01111-61902	SWITCH ASSEMBLY	
C1	0150-0096	C:FXD CER 0.05 UF 100VDCW	
C2 AND C3		NOT ASSIGNED	
C4	01111-80701	ASSY:CAPACITOR 2000 UF	
C5	0150-0121	C:FXD CER 0.1 UF +80-20% 50VDCW	
C6		N.S.R PART OF A2	
C7 AND C8	0180-0059	C:FXD ELECT 10 UF +100-10% 25VDCW	
C9	0150-0121	C:FXD CER 0.1 UF +80-20% 50VDCW	
C10		NOT ASSIGNED	
C11	0121-0037	C:VAR CER 7-25 PF N300	
C12	0121-0037	C:VAR CER 7-25 PF N300	
C13	0132-0005	C:VAR POLY 0.7-3.0 PF 350VDCW	
C14	0150-0121	C:FXD CER 0.1 UF +80-20% 50VDCW	
C15		NOT ASSIGNED	
C16	0150-0121	C:FXD CER 0.1 UF +80-20% 50VDCW	
C17	0150-0121	C:FXD CER 0.1 UF +80-20% 50VDCW	
C18	0180-0076	CFXD ELECT 20 UF 25VDCW	
C19	0150-0073	C:FXD CER 100 PF 10% 500VDCW	
C20	0160-0128	C:FXD CER 2.2 UF 20% 25VDCW	
C21	0150-0121	C:FXD CER 0.1 UF +80-20% 50VDCW	
C22 THRU C24		NOT ASSIGNED	
C25	0150-0096	C:FXD CER 0.05 UF 100VDCW	
C26	0150-0096	C:FXD CER 0.05 UF 100VDCW	
C27	0180-0138	C:FXD ELECT 100 UF +100-10% 40VDCW	
C28	0180-0138	C:FXD ELECT 100 UF +100-10% 40VDCW	
C29	0180-0049	C:FXD ELECT 20 UF 50VDCW	
C30 THRU C31		NOT ASSIGNED	
C32	0180-0059	C:FXD ELECT 10 UF +100-10% 25VDCW	
C33	0180-0104	C:FXD ELECT 200 UF 15VDCW	
C34	0180-0104	C:FXD ELECT 200 UF 15VDCW	
CR1 THRU CR4	1901-0025	SEMICON DEVICE:DIODE SILICON	
CR5 AND CR6		NOT ASSIGNED	
CR7	1902-0025	SEMICON DEVICE:DIODE ZENER 10V	
CR8 AND CR9		NOT ASSIGNED	
CR10	1902-0078	SEMICON DEVICE:DIODE ZENER 14.7V	
J1	1250-0123	CONNECTOR:FEMALE BNC	
J2	1250-0123	CONNECTOR:FEMALE BNC	
L1	9170-0016	SHIELDING BEAD	
P1	1251-0348	PLUG 125VOLT	

= See list of abbreviations in introduction to this section

Table 6-1. Reference Designation Index (Cont'd)

Reference Designation	Stock No.	Description #	Note
Q1 THRU			
Q4	1850-0075	TRANSISTOR:GERMANIUM PNP 2N779A	
Q5	1854-0019	TRANSISTOR:SILICON NPN 2N2368	
Q6	1854-0003	TRANSISTOR:SILICON NPN	
R1	0727-0899	R:FXD DEPC .5 OHM 2% 1/2W	
R2	0721-0028	R:FXD DEPC 48.7 OHM 1% 1/8W	
R3		NOT ASSIGNED	
R4	0699-0001	R:FXD COMP 2.7 OHM 10% 1/2W	
R5	0683-2425	R:FXD COMP 2400 OHM 5% 1/4W	
R6	0683-1025	R:FXD COMP 1K OHM 5% 1/4W	
R7	0683-2725	R:FXD COMP 2.7K OHM 5% 1/4W	
R8	0683-1225	R:FXD COMP 1.2K OHM 5% 1/4W	
R9 AND		NOT ASSIGNED	
R10			
R11	0683-3325	R:FXD COMP 3.3K OHM 5% 1/4W	
R12	0683-1235	R:FXD COMP 12K OHM 5% 1/4W	
R13	0683-2705	R:FXD COMP 27 OHM 5% 1/4W	
R14	2100-0090	R:VAR COMP 2000 OHM 30% LIN 1/3W	
R15	0683-2015	R:FXD COMP 200 OHM 5% 1/4W	
R16 AND	0683-5125	R:FXD COMP 5.1K OHM 5% 1/4W	
R17	0683-4715	R:FXD COMP 470 OHM 5% 1/4W	
R18 AND	0727-0116	NOT ASSIGNED R:FXD DEPC 2.03K OHM 1% 1/2W	
R19			
R20			
R21	0727-0100	R:FXD DEPC 1K OHM 1% 1/2W	
R22	0727-0072	R:FXD DEPC 403 OHM 1% 1/2W	
R23	0727-0055	R:FXD DEPC 201 OHM 1% 1/2W	
R24 AND		NOT ASSIGNED	
R27			
R28 AND	0727-0023	R:FXD DEPC 50 OHM 1% 1/2W	
R29	0727-0055	R:FXD DEPC 201 OHM 1% 1/2W	
R30 AND		NOT ASSIGNED	
R31			
R32	0683-1035	R:FXD COMP 10K OHM 5% 1/4W	
R33 AND	0686-2015	R:FXD COMP 200 OHM 5% 1/2W	
R34	0727-0709	R:FXD DEPC 15.4 OHM 5% 1/2W	
R35	0683-1515	R:FXD COMP 150 OHM 5% 1/4W	
R36 AND		NOT ASSIGNED	
R37			
R38 THRU	0683-8225	R:FXD COMP 8.2K OHM 5% 1/4W	
R39	0683-3625	R:FXD COMP 3.6K OHM 5% 1/4W	
R40	2100-0151	R:VAR COMP 500 OHM 20% LIN 2/10W	
R41	0727-0031	R:FXD DEPC 60 OHM 1% 1/2W	
R42 AND		NOT ASSIGNED	
R44			
R45	0687-1821	R:FXD COMP 1.8K OHM 10% 1/2W	
R46	0687-1821	R:FXD COMP 1.8K OHM 10% 1/2W	
R47	0760-0027	R:FXD MET OX 150 OHM 2% 1W	
R48	0687-1021	R:FXD COMP 1K OHM 10% 1/2W	
S1	3101-0033	SWITCH:SLIDE DPDT(115-230V)	
S2	3101-0070	SWITCH:SLIDE DPDT	
S3		N.S.R. PART OF A3	
T1	9100-0183	TRANSFORMER:POWER	

# See list of abbreviations in introduction to this section

Table 6-1. Reference Designation Index (Cont'd)

Reference Designation	Stock No.	Description #	Note
W1	01111-61601	CABLE:POWER  MISCELLANEOUS  5000-0023 5000-0101 5060-0213 1205-0011  0370-0104 01111-00201 01111-46101 BODY:CABINET COVER:CABINET SIDE FRAME:CABINET SIDE HEAT SINK  KNOB: SENSITIVITY PANEL TERMINAL BOOT-CABLE	

= See list of abbreviations in introduction to this section

Table 6-2. Replaceable Parts

Stock No.	Description #	Mfr.	Mfr. Part No.	TQ
0121-0037	C:VAR CER 7-25 PF N300	28480	0121-0037	2
0132-0005	C:VAR POLY 0.7-3.0 PF 350VDCW	72982	535-031-4R	1
0150-0073	C:FXD CER 100 PF 10% 500VDCW	56289	40C 200A2	1
0150-0096	C:FXD CER 0.05 UF 100VDCW	91418	TA	3
0150-0121	C:FXD CER 0.1 UF +80-20% 50VDCW	56289	5C50A	6
0160-0128	C:FXD CER 2.2 UF 20% 25VDCW	56289	5C15	1
0180-0049	C:FXD ELECT 20 UF 50VDCW	56289	D33909	1
0180-0059	C:FXD ELECT 10 UF +100-10% 25VDCW	56289	300 106G 025	2
0180-0076	C:FXD ELECT 20 UF 25VDCW	56289	400 181 A2	1
0180-0104	C:FXD ELECT 200 UF 15VDCW	56289	300 174 A1	2
0180-0138	C:FXD ELECT 100 UF +100-10% 40VDCW	56289	D36254	2
0370-0104	KNOB: SENSITIVITY	28480	0370-0104	1
0683-1025	R:FXD COMP 1K OHM 5% 1/4W	01121	CB 1025	1
0683-1035	R:FXD COMP 10K OHM 5% 1/4W	01121	CB 1035	1
0683-1225	R:FXD COMP 1.2K OHM 5% 1/4W	01121	CB 1225	1
0683-1235	R:FXD COMP 12K OHM 5% 1/4W	01121	CB 1235	1
0683-1515	R:FXD COMP 150 OHM 5% 1/4W	01121	CB 1515	1
0683-2015	R:FXD COMP 200 OHM 5% 1/4W	01121	CB 2015	1
0683-2425	R:FXD COMP 2400 OHM 5% 1/4W	01121	CB 2425	1
0683-2705	R:FXD COMP 27 OHM 5% 1/4W	01121	CB 2705	1
0683-2725	R:FXD COMP 2.7K OHM 5% 1/4W	01121	CB 2725	1
0683-3325	R:FXD COMP 3.3K OHM 5% 1/4W	01121	CB 3325	1
0683-3625	R:FXD COMP 3.6K OHM 5% 1/4W	01121	CB 3625	1
0683-4715	R:FXD COMP 470 OHM 5% 1/4W	01121	CB 4715	1
0683-5125	R:FXD COMP 5.1K OHM 5% 1/4W	01121	CB 5125	1
0683-8225	R:FXD COMP 8.2K OHM 5% 1/4W	01121	CB 8225	1
0686-2015	R:FXD COMP 200 OHM 5% 1/2W	01121	EB 2015	1
0687-1021	R:FXD COMP 1K OHM 10% 1/2W	01121	EB 1021	1
0687-1821	R:FXD COMP 1.8K OHM 10% 1/2W	01121	EB 1821	2
0699-0001	R:FXD COMP 2.7 OHM 10% 1/2W	01121	EB 2761	1
0721-0028	R:FXD DEPC 48.7 OHM 1% 1/8W	19701	DC 1/8A	1
0727-0023	R:FXD DEPC 50 OHM 1% 1/2W	19701	DC 1/2C	1
0727-0031	R:FXD DEPC 60 OHM 1% 1/2W	19701	DC 1/2C	1
0727-0055	R:FXD DEPC 201 OHM 1% 1/2W	19701	DC 1/2C	2
0727-0072	R:FXD DEPC 403 OHM 1% 1/2W	19701	DC 1/2C	1
0727-0100	R:FXD DEPC 1K OHM 1% 1/2W	19701	DC 1/2C	1
0727-0116	R:FXD DEPC 2.03K OHM 1% 1/2W	19701	DC 1/2C	1
0727-0709	R:FXD DEPC 15.4 OHM 5% 1/2W	19701	DC 1/2A	1
0727-0899	R:FXD DEPC .5 OHM 2% 1/2W	28480	0727-0899	1
0760-0027	R:FXD MET OX 150 OHM 2% 1W	07115	C32	1
01111-00201	PANEL	28480	01111-00201	1
01111-46101	TERMINAL BOOT-CABLE	28480	01111-46101	1
01111-61601	CABLE:POWER	28480	01111-61601	1
01111-61902	SWITCH ASSEMBLY	28480	01111-61902	1
01111-66502	AMPLIFIER ASSEMBLY	28480	01111-66502	1
01111-67601	POWER PLUG ASSEMBLY	28480	01111-67601	1
01111-80701	ASSY:CAPACITOR 2000 UF	28480	01111-80701	1
1205-0011	HEAT SINK	28480	1205-0011	1
1250-0123	CONNECTOR:FEMALE BNC	91737	UG-1094/U	2

= See list of abbreviations in introduction to this section

Table 6-2. Replaceable Parts (Con't)

Stock No.	Description #	Mfr.	Mfr. Part No.	TQ
1251-0348	PLUG 125 VOLT	02660	160-11	
1850-0075	TRANSISTOR:GERMANIUM PNP 2N779A	87216	2N779A	1
1854-0003	TRANSISTOR:SILICON NPN	28480	1854-0003	1
1854-0019	TRANSISTOR:SILICON NPN 2N2368	07263	2N2368	1
1901-0025	SEMICON DEVICE:DIODE SILICON	28480	1901-0025	4
1902-0025	SEMICON DEVICE:DIODE ZENER 10V	28480	1902-0025	1
1902-0078	SEMICON DEVICE:DIODE ZENER 14.7V	28480	1902-0078	1
2100-0090	R:VAR COMP 2000 OHM 30% LIN 1/3W	28480	2100-0090	1
2100-0151	R:VAR COMP 5000OHM 20% LIN 1/5W	28480	2100-0151	1
3101-0033	SWITCH:SLIDE DPDT (115-230V)	42190	4633	1
3101-0070	SWITCH:SLIDE DPDT	79727	126-B	1
5000-0023	BODY:CABINET	28480	5000-0023	1
5000-0101	COVER:CABINET SIDE	28480	5000-0101	2
5060-0213	FRAME:CABINET SIDE	28480	5060-0213	2
9100-0183	TRANSFORMER:POWER	28480	9100-0183	1
9170-0016	SHIELDING BEAD	28480	9170-0016	1

# See introduction to this section

**TABLE 6-3. CODE LIST OF MANUFACTURERS**

The following code numbers are from the Federal Supply Code for Manufacturers Cataloging Handbooks H4-1 (Name to Code) and H4-2 (Code to Name) and their latest supplements. The date of revision and the date of the supplements used appear at the bottom of each page. Alphabetical codes have been arbitrarily assigned to suppliers not appearing in the H4 handbooks.

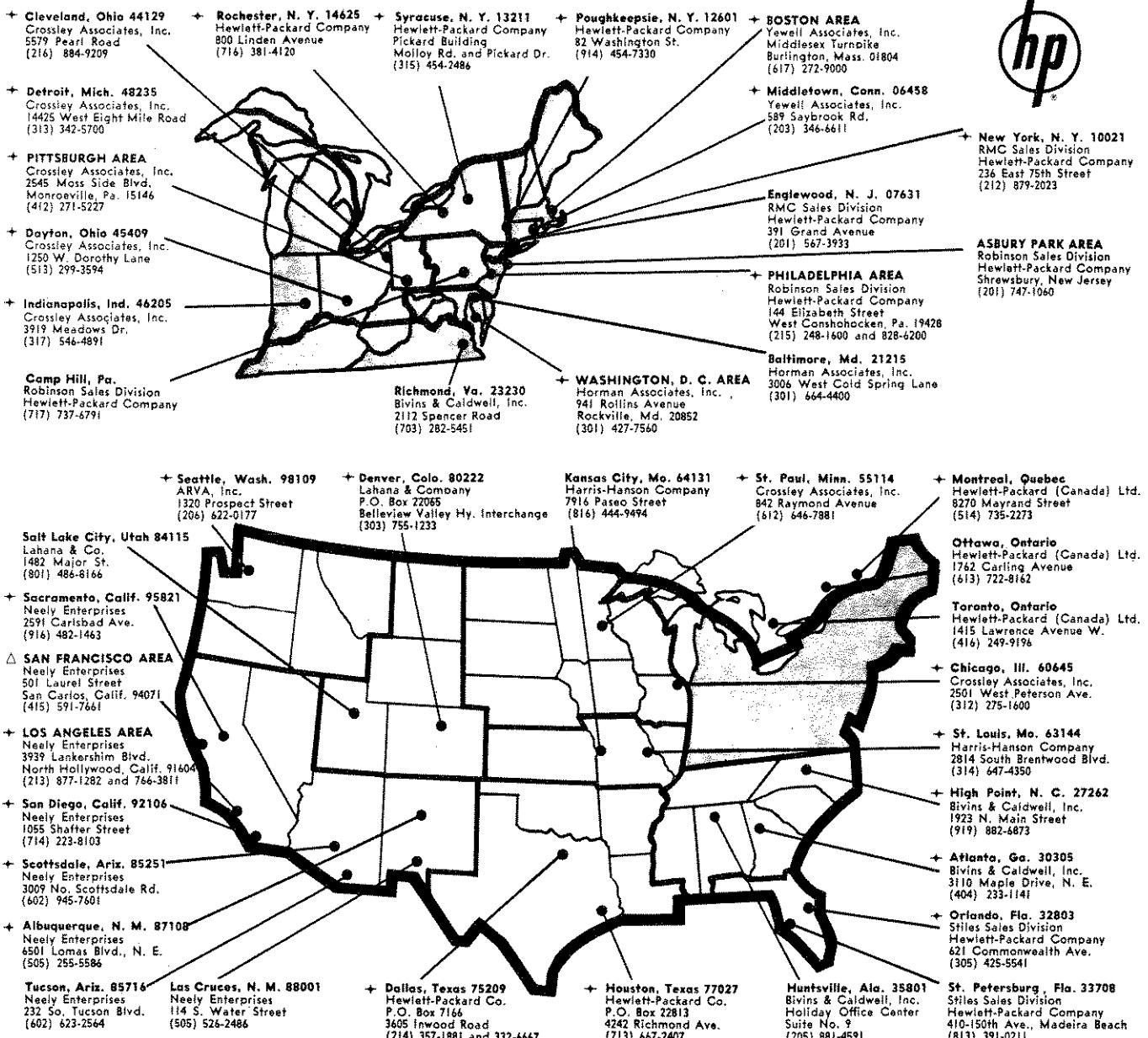
Code No.	Manufacturer	Address	Code No.	Manufacturer	Address	Code No.	Manufacturer	Address	Code No.	Manufacturer	Address
00008 U.S.A. Common	Any supplier of U.S.		07263 Fairchild Semiconductor Corp.	Mountain View, Calif.		63743 Ward Leonard Electric	Mt. Vernon, N.Y.		74861 Industrial Condenser Corp.	Chicago, Ill.	
00136 McCoy Electronics	Mount Holly Springs, Pa.		07322 Minnesota Rubber Co.	Minneapolis, Minn.		54294 Shalcross Mfg. Co.	Selma, N.C.		74862 R.F. Products Division of Amphenol	Banbury, Conn.	
00334 Humidair Co.	Cotton, Calif.		07700 Technical Wire Products	Springfield, N.J.		55026 Simpson Electric Co.	Chicago, Ill.		74970 Borg Electronics Corp.	Waseca, Minn.	
00335 Westrex Corp.	New York, N.Y.		07910 Continental Device Corp.	Hawthorne, Calif.		55932 Sonotone Corp.	Erlton, N.Y.		75042 E.F. Johnson Co.	Philadelphia, Pa.	
00373 Galco Packing Co., Electronic Products Div.	Camden, N.J.		07933 Rheem Semiconductor Corp.	Mountain View, Calif.		56137 Spaulding Fibre Co., Inc.	Torawanda, N.Y.		75173 International Resistance Co.	Philadelphia, Pa.	
00656 Astrotron Corp.	New Bedford, Mass.		07966 Shockley Semi-Conductor Laboratories	Palo Alto, Calif.		56295 Sprague Electric Co.	North Adams, Mass.		75174 Jones, Howard B., Division of Cinch Mfg. Corp.	Chicago, Ill.	
00779 Amp, Inc.	Harrisburg, Pa.		07980 Boatman Radio Corp.	Boonton, N.J.		59446 Telex, Inc.	St. Paul, Minn.		75178 James Knight Co.	Sandwich, Ill.	
00781 Aircraft Radio Corp.	Boonton, N.J.		08145 U.S. Engineering Co.	Los Angeles, Calif.		59730 Thomas & Betts Co.	Elizabeth, N.J.		75230 Kulka Electric Corporation	Mt. Vernon, N.Y.	
00815 Northern Engineering Laboratories, Inc.	Burlington, Wis.		08358 Burgess Battery Co.	Niagara Falls, Ontario, Canada		60741 Tippett Electrical Inc.	Bluffton, Ohio		75818 Lenx Electric Mfg. Co.	Chicago, Ill.	
00853 Sangamo Electric Company, Orillia Division (Capacitors)	Marion, Ill.		08717 Sloan Company	Burbank, Calif.		61775 Union Switch and Signal, Div. of Westinghouse Air Brake Co.	Swissvale, Pa.		75919 Littlefuse Inc.	Ges Flaines, Ill.	
00886 Gee Engineering Co.	Los Angeles, Calif.		08718 Cannon Electric Co., Phoenix Div.	Phoenix, Ariz.		62119 Universal Electric Co.	Owosso, Mich.		76005 Lord Mfg. Co.	Erie, Pa.	
00891 Carl E. Holmes Corp.	Los Angeles, Calif.		08792 CBS Electronics Semiconductor Operations, Div. of C.B.S., Inc.	Lowell, Mass.		63743 Ward-Leonard Electric Co.	Mt. Vernon, N.Y.		76710 C.W. Marwedel	San Francisco, Calif.	
01121 Allen Bradley Co.	Milwaukee, Wis.		08984 Mel-Ray	Indianapolis, Ind.		64955 Western Electric Co., Inc.	New York, N.Y.		76833 Micromold Electronic Mfg. Corp.	Brooklyn, N.Y.	
01255 Litton Industries, Inc.	Beverly Hills, Calif.		09026 Babcock Relays, Inc.	Costa Mesa, Calif.		65092 Weston Inst. Div. of Daystrom, Inc.	Newark, N.J.		76481 James Miller Mfg. Co., Inc.	Malden, Mass.	
01281 Pacific Semiconductors, Inc.	Culver City, Calif.		09134 Texas Capacitor Co.	Houston, Texas		65295 Wittek Manufacturing Co.	Chicago 23, Ill.		76483 J.W. Miller Co.	Los Angeles, Calif.	
01295 Texas Instruments, Inc.			09250 Electro Assemblies, Inc.	Chicago, Ill.		65345 Wollensak Optical Co.	Rochester, N.Y.		76530 Monadnock Mills	San Leandro, Calif.	
01349 The Allis-Chalmers Mfg. Co.	Dallas, Texas		09569 Mallory Battery Co., Ltd.	Toronto, Ontario, Canada		70276 Allen Mfg. Co.	Harford, Conn.		76545 Mueller Electric Co.	Cleveland, Ohio.	
01561 Chaser-Trak Corp.	Alliance, Ohio		09589 The Bristol Co.	Waterbury, Conn.		70308 Allied Control Co., Inc.	New York, N.Y.		76564 Oak Manufacturing Co.	Crystal Lake, Ill.	
01589 Pacific Relays, Inc.	Indianapolis, Ind.		10214 General Transistor Western Corp.	Los Angeles, Calif.		70319 Allmetal Screw Prod. Co., Inc.	Bendix Corp.		77068 Bendix Pacific Division of	No. Hollywood, Calif.	
01930 Amerock Corp.	Rockford, Ill.		10411 Tri-Tat, Inc.	Berkeley, Calif.		70485 Atlantic India Rubber Works, Inc.	Chicago, Ill.		77075 Pacific Metals Co.	San Francisco, Calif.	
01961 Pulse Engineering Co.	Santa Clara, Calif.		10646 Carbonumond Co.	Niagara Falls, N.Y.		70563 Amperite Co., Inc.	New York, N.Y.		77221 Phosfon Instrument and Electronic Co.	South Pasadena, Calif.	
02114 Ferriscube Corp. of America	Saugerties, N.Y.		11236 CTS of Berne, Inc.	Berne, Ind.		70903 Belden Mfg. Co.	Chicago, Ill.		77250 Phenix Mfg. Co.	Chicago, Ill.	
02286 Cole Mfg. Co.	Palo Alto, Calif.		11237 Chicago Telephone of California, Inc.	So. Pasadena, Calif.		71002 Bird Electronic Corp.	Cleveland, Ohio		77252 Philadelphia Steel and Wire Corp.	Philadelphia, Pa.	
02660 Amphenol-Borg Electronics Corp.	Chicago, Ill.		11312 Microwave Electronics Corp.	Palo Alto, Calif.		71041 Birnbach Radio Co.	New York, N.Y.		77342 Potter and Brumfield, Div. of American Machine and Foundry	Princeton, Ind.	
02735 Radio Corp. of America, Semiconductor and Materials Div.	Somerville, N.J.		11532 Duncan Electronic, Inc.	Santa Ana, Calif.		71128 Bud Radio Inc.	Cleveland, Ohio		77630 Radio Condenser Co.	Camden, N.J.	
02771 Vocaline Co. of America, Inc.	Old Saybrook, Conn.		11711 General Instrument Corporation Semiconductor Division	Newark, N.J.		71285 Camloc Fastener Corp.	Paramus, N.J.		77635 Radio Receptor Co., Inc.	Brooklyn, N.Y.	
02777 Hopkins Engineering Co.	San Fernando, Calif.		11717 Imperial Electronic, Inc.	Buena Park, Calif.		71313 Allen B. Cardwell Electronic Prod. Corp.	Plainville, Conn.		77764 Resistance Products Co.	Harrisburg, Pa.	
03508 G.E. Semiconductor Products Dept.	Syracuse, N.Y.		11870 Melabs, Inc.	Palo Alto, Calif.		71400 Bussmann Fuse Div. of McGraw- Edison Co.	St. Louis, Mo.		78189 Shakeproof Division of Illinois Tool Works	Elgin, Ill.	
03705 Apex Machine & Tool Co.	Dayton, Ohio		12697 Clarcstat Mfg. Co.	Dover, N.H.		71435 Chicago Condenser Corp.	Chicago, Ill.		78283 Signal Indicator Corp.	New York, N.Y.	
03787 Eldena Corp.	El Monte, Calif.		12859 Nippon Electric Co., Ltd.	Tokyo, Japan		71450 CTS Corp.	Elkhart, Ind.		78290 Strothers-Dunn Inc.	Pittman, N.J.	
03888 Transition Electronic Corp.	Wakefield, Mass.		12930 Delta Semiconductor Inc.	Newport Beach, Calif.		71468 Cannon Electric Co.	Los Angeles, Calif.		78452 Thompson-Bremer & Co.	Chicago, Ill.	
03954 Aerial Marine Motors, Inc.	Monstition, N.J.		13103 Thermoloy	Dallas, Texas		71471 Cinema Engineering Co.	Burbank, Calif.		78471 Tilley Mfg. Co.	San Francisco, Calif.	
04009 Arrow, Hart and Hegeman Elect. Co.	Hartford, Conn.		13396 Telefunken (G.M.B.H.)	Hannover, Germany		71482 C.P. Clark & Co.	Chicago, Ill.		78488 Stackpole Carbon Co.	St. Marys, Pa.	
04062 Elmetco Products Co.	New York, N.Y.		14099 Sem-Tech	Newbury Park, Calif.		71500 Centralab Div. of Globe Union Inc.	Milwaukee, Wis.		78493 Standard Thomson Corp.	Walham, Mass.	
04222 Hi-Q Division of Aerovox	Myrtle Beach, S.C.		14193 Calif. Resistor Corp.	Santa Monica, Calif.		71708 The Cornish Wire Co.	New York, N.Y.		78553 Timmerman Products, Inc.	Cleveland, Ohio.	
04238 Elgin National Watch Co., Electronics Division	Burbank, Calif.		14298 American Components, Inc.	Coateshocker, Pa.		71744 Chicago Miniature Lamp Works	Chicago, Ill.		78730 Transformer Engineers	Pasadena, Calif.	
04404 Dymer Division of Hewlett-Packard Co.	Palo Alto, Calif.		14655 Canfield Ballistic Elec. Corp.	So. Plainfield, N.J.		71753 A.O. Smith Corp., Crowley Div.	West Orange, N.J.		78947 Unicore Co.	Newtonville, Mass.	
04651 Sylvania Electric Prods., Inc., Electronic Tube Div.	Mountain View, Calif.		15090 The Daven Co.	Livingston, N.J.		71785 Cinch Mfg. Corp.	Chicago, Ill.		79142 Veedol Reel, Inc.	Hartford, Conn.	
04713 Motorola, Inc., Semiconductor Prod. Div.	Phoenix, Arizona		16688 De Jui-Anasco Corporation	Long Island City 1, N.Y.		71984 Dow Corning Corp.	Midland, Mich.		79251 Wecco Mfg. Co.	Chicago, Ill.	
04732 Filtron Co., Inc., Western Div.	Culver City, Calif.		16758 Delco Radio Div. of G.M. Corp.	Kokomo, Ind.		72092 Estele-McCullough, Inc.	San Bruno, Calif.		79727 Continental-Wirt Electronics Corp.	Philadelphia, Pa.	
04773 Automatic Electric Co.	Northlake, Ill.		18873 E.I. DuPont and Co., Inc.	Wilmington, Del.		72136 Electro Molyb. Mfg. Co., Inc.	Willimantic, Conn.		79963 Zierick Mfg. Corp.	New Rochelle, N.Y.	
04777 Automatic Electric Sales Corp.	Northgate, N.J.		19315 Eclipse Pioneer, Div. of Bendix Aviation Corp.	Teterboro, N.J.		72170 Coto Coil Co., Inc.	Providence, R.I.		80031 Meaco Division of Sessions Sleek Co.	Morristown, N.J.	
04796 Sequira Wire & Cable Co.	Redwood City, Calif.		19500 Thomas A. Edison Industries, Div. of McGraw-Edison Co.	West Orange, N.J.		72354 John E. Fast & Co.	Chicago, Ill.		80707 Schnitzer Alloy Products	Elizabeth, N.J.	
04870 P. M. Motor Company	Chicago 44, Ill.		19701 Electra Manufacturing Co.	Kansas City, Mo.		72519 Dialight Corp.	Brooklyn, N.Y.		80130 Times Facsimile Corp.	New York, N.Y.	
05006 Twentieth Century Plastics, Inc.	Los Angeles, Calif.		20183 Electronic Tube Corp.	Philadelphia, Pa.		72625 General Ceramics Corp.	Keasbey, N.J.		80131 Electronic Industries Association	Any brand	
05277 Westinghouse Electric Corp., Semiconductor Dept.	Youngwood, Pa.		21226 Executive, Inc.	New York, N.Y.		72659 General Instrument Corp., Semiconductor Div.	Newark, N.J.		80207 Unimax Switch, Div. of W.L. Marson Corp.	Wattingford, Conn.	
05347 Ultironix, Inc.	San Mateo, Calif.		21335 The Fafnir Bearing Co.	New Britain, Conn.		72738 Guard-Hopkins	Oakland, Calif.		80223 United Transformer Corp.	New York, N.Y.	
05593 Illumintron Engineering Co.	Sunnyvale, Calif.		21964 Fed. Telephone and Radio Corp.	Clifton, N.J.		72765 Drake Mfg. Co.	Chicago, Ill.		80248 Oxford Electric Corp.	Chicago, Ill.	
05624 Barber Colman Co.	Rockford, Ill.		22446 General Electric Co.	Schenectady, N.Y.		72825 Hughes H. Eby Inc.	Philadelphia, Pa.		80294 Bourne Laboratories, Inc.	Riverside, Calif.	
05728 Tiffen Optical Co.	Roslyn Heights, Long Island, N.Y.		24455 General Radio Co.	West Concord, Mass.		72925 Gudeman Co.	Chicago, Ill.		80411 Fulton Controls Co.	Columbus 16, Ohio	
05729 Metropolitan Telecommunications Corp., Metho Cap. Division	Brooklyn, N.Y.		26365 Gries Reproducer Corp.	New Rochelle, N.Y.		72992 Elrite Resistor Corp.	Los Angeles, Calif.		80486 All Star Products Inc.	Delaware, Ohio	
05783 Stewart Engineering Co.	Santa Cruz, Calif.		26462 Grobel Film Co. of America, Inc.	Carlstadt, N.J.		73061 Hansen Mfg. Co., Inc.	Erie, Pa.		80563 Hammerlund Co., Inc.	New York, N.Y.	
06004 The Bassick Co.	Bridgeport, Conn.		26992 Hamilton Watch Co.	Lancaster, Pa.		73076 H.M. Haiper Co.	Princeton, Ind.		80640 Stevens, Arnold, Co., Inc.	Boston, Mass.	
06175 Baush and Lomb Optical Co.	Rochester, N.Y.		28480 Hewlett-Packard Co.	Palo Alto, Calif.		73138 Helipot Div. of Beckman Instruments, Inc.	Chicago, Ill.		81030 International Instruments, Inc.	New Haven, Conn.	
06402 E.T.A. Products Co. of America	Chicago, Ill.		35173 G.E. Receiving Tube Dept.	Owensboro, Ky.		73293 Hughes Products Division of Hughes Aircraft Co.	Newport Beach, Calif.		81073 Grayhill Co.	LaGrange, Ill.	
06555 Beede Electrical Instrument Co., Inc.	Penacook, N.H.		35434 Lectron Inc.	Chicago, Ill.		73445 Amperex Electronic Co., Div. of North American Philips Co. Inc.	Hicksville, N.Y.		81095 Triad Transformer Corp.	Venice, Calif.	
06751 U.S. Semcor Division of Nuclear Corp. of America	Phoenix, Arizona		37942 P.R. Mallory & Co., Inc.	Indianapolis, Ind.		73490 Beckman Helipot Corp.	So. Pasadena, Calif.		81312 Winchester Electronics Co., Inc.	Newark, Conn.	
06812 Torrington Mfg. Co., West Div.	Van Nuys, Calif.		40920 Miniature Precision Bearings, Inc.	Keene, N.H.		73506 Bradley Semiconductor Corp.	Hamden, Conn.		81349 Military Specification	.....	
07115 Corning Glass Works	Electronic Components Dept.		42190 Muter Co.	Chicago, Ill.		73559 Carling Electric, Inc.	Harford, Conn.		81415 Wilkow Products, Inc.	Cleveland, Ohio	
07126 Digitron Co.	Bradford, Pa.		43590 C.A. Morgan Co.	Englewood, Colo.		73682 George K. Garrett Co., Inc.	Philadelphia, Pa.		81451 Raytheon Mfg. Co., Industrial Components Div., Indust. Tube Operations	Newtown, Mass.	
07137 Transistor Electronics Corp.	Minneapolis, Minn.		44655 Ohmite Mfg. Co.	Skokie, Ill.		73734 Federal Screw Prod. Co.	Chicago, Ill.		81483 International Rectifier Corp.	El Segundo, Calif.	
07138 Westinghouse Electric Corp., Electronic Tube Div.	Erlina, N.Y.		47904 Polaroid Corp.	Cambridge, Mass.		73743 Fischer Special Mfg. Co.	Cincinnati, Ohio		81541 The Alpha Products Co.	Cambridge, Mass.	
07261 Avnet Corp.	Los Angeles, Calif.		48620 Precision Thermometer and Inst. Co.	Philadelphia, Pa.		73783 The General Industries Co.	Elyria, Ohio		81860 Barry Controls, Inc.	Watertown, Mass.	
			49956 Raytheon Company	Lexington, Mass.		73905 Jennings Radio Mfg. Co.	San Jose, Calif.		82042 Carter Parts Co.	Skokie, Ill.	
			52090 Rowan Controller Co.	Baltimore, Md.		74455 J.H. Winns, and Sons	Winchester, Mass.		82142 Jeffrey Electronics Division of Speer Carbon Co.	Du Bois, Pa.	
									82170 Allen B. DuMont Labs, Inc.	Clifton, N.J.	

TABLE 6-3. CODE LIST OF MANUFACTURERS (CONT'D)

Code No.	Manufacturer	Address	Code No.	Manufacturer	Address	Code No.	Manufacturer	Address	Code No.	Manufacturer	Address
82269	Maguire Industries, Inc.	Greenwich, Conn.	88220	Gould-National Batteries, Inc.	St. Paul, Minn.	95238	Continental Connector Corp.	Woodside, N.Y.	00000	JFD Electronics Corp.	Van Nuys, Calif.
82279	Sylvania Electric Prod., Inc.	Emporium, Pa.	88698	General Mills, Inc.	Buffalo, N.Y.	95263	Leecraft Mfg. Co., Inc.	New York, N.Y.	00000	Tranex Company	Mountain View, Calif.
82278	Electronic Tube Div.	East Newark, N.J.	89231	Graybar Electric Inc., Co.	Oakland, Calif.	95264	Lerco Electronics, Inc.	Burbank, Calif.	10090	Western Devices, Inc.	Inglewood, Calif.
82275	Aston Co.	Chicago, Ill.	89473	General Electric Distributing Corp.	Schenectady, N.Y.	95265	National Coil Co.	Sheridan, Wyo.	10090	Winchester Electronics, Inc.	Santa Monica, Calif.
82283	Switchcraft, Inc.		89536	Carter Parts Div. of Economy Baler Co.	Chicago, Ill.	95275	Vitramon, Inc.	Bridgeport, Conn.	0000F	Marco Tool and Die Ind., Inc.	Los Angeles, Calif.
82647	Metals and Controls, Inc., Div. of Texas Instruments, Inc., Spencer Prods.	Attleboro, Mass.	89665	United Transformer Co.	Chicago, Ill.	95348	Gordas Corp.	Bloomfield, N.J.	0000M	Western Coil Div. of Automatic	Redwood City, Calif.
87966	Research Products Corp.	Madison, Wis.	90179	U.S. Rubber Co., Mechanical Goods Div.	Passaic, N.J.	95354	Methode Mfg. Co.	Chicago, Ill.	0000N	Nahm-Bros. Spring Co.	San Leandro, Calif.
82877	Rotom Manufacturing Co., Inc.	Woodstock, N.Y.	90970	Bearing Engineering Co.	San Francisco, Calif.	95987	Weckesel Co.	Chicago, Ill.	0000O	U.S.A. Common	Any supplier of U.S.
82955	Vector Electronic Co.	Glenelg, Calif.	91261	Connor Spring Mfg. Co.	San Francisco, Calif.	96067	Huggins Laboratories	Sunnyvale, Calif.	0000P	Ty-Car Mfg. Co., Inc.	Holliston, Mass.
83053	Western Washer Mfg. Co.	Los Angeles, Calif.	91343	Milner Dial & Nameplate Co.	El Monte, Calif.	96256	Thordarson-Messmer Div. of Maguire Industries, Inc.	Mt. Carmel, Ill.	0000T	Texas Instruments, Inc., Metals and Controls Div.	Versailles, Ky.
83058	Car Fastener Co.	Cambridge, Mass.	91416	Radio Materials Co.	Chicago, Ill.	96286	Solaris Manufacturing Co.	Los Angeles, Calif.	0000U	Tower Mfg. Corp.	Providence, R.I.
83085	New Hampshire Ball Bearing, Inc.	Peterborough, N.H.	91508	Augat Brothers', Inc.	Attleboro, Mass.	96330	Carlton Screw Co.	Chicago, Ill.	0000W	Webster Electronics Co., Inc.	New York, N.Y.
83125	Pyramid Electric Co.	Dartington, S.C.	91637	Date Electronics, Inc.	Columbus, Nebr.	96341	Microwave Associates, Inc.	Burlington, Mass.	0000X	Spruce Pine Mica Co.	Spruce Pine, N.C.
83148	Electric Cords Co.	Los Angeles, Calif.	91662	Eico Corp.	Philadelphia, Pa.	96501	Excel Transformer Co.	Oakland, Calif.	0000Y	Midland Mfg. Co., Inc.	Kansas City, Kans.
83166	Victory Engineering Corp.	Union, N.J.	91737	Gremar Mfg. Co., Inc.	Wakefield, Mass.	97464	Industrial Retaining Ring Co.	Irvington, N.J.	0000Z	Willow Leather Products Corp.	Newark, N.J.
83215	Bendix Corp., Red Bank Div.	Red Bank, N.J.	91827	K F Development Co.	Redwood City, Calif.	97539	Automatic and Precision Mfg. Co.	Yonkers, N.Y.	000AA	British Radio Electronics Ltd.	Washington, D.C.
83215	Hubbell Corp.	Mundelein, Ill.	91929	Minneapolis-Honeywell Regulator Co., Microswitch Div.	Freeport, Ill.	97966	CBS Electronics, Div. of C.B.S., Inc.	Danvers, Mass.	000AB	ETA	England
83330	Smith, Herman H., Inc.	Brooklyn, N.Y.	92196	Universal Metal Prod., Inc.	Bassett Puebla, Calif.	97979	Reem Resistor Corp.	Yonkers, N.Y.	000AC	Indiana General Corp., Elect. Div.	Indiana
83385	Central Screw Co.	Chicago, Ill.	92367	Elgeet Optical Co., Inc.	Rochester, N.Y.	98141	Axel Brothers Inc.	Jamaica, N.Y.	000AD	Curtis Instrument Inc.	Mt. Kisco, N.Y.
83501	Gavitt Wire and Cable Co., Div. of America Corp.	Brookfield, Mass.	92697	Tinselite Insulated Wire Co.	Tarrytown, N.Y.	98159	Rubber Tech, Inc.	Gardena, Calif.	000BB	Precision Instrument Components Co.	Van Nuys, Calif.
83594	Burroughs Corp.		93322	Sylvania Electric Prod., Inc., Semiconductor Div.	Woburn, Mass.	98220	Francis L. Mosley	Pasadena, Calif.	000CC	Computer Diode Corp.	Lodi, N.J.
	Electronic Tube Div.	Plainfield, N.J.	93369	Robbins and Myers, Inc.	New York, N.Y.	98278	Microdot, Inc.	So. Pasadena, Calif.	000EE	A. Williams Manufacturing Co.	San Jose, Calif.
83740	Eveready Battery	New York, N.Y.	93410	Stevens Mfg. Co., Inc.	Mansfield, Ohio	98291	Sealecito Corp.	Mamaroneck, N.Y.	000GG	Goshen Die Cutting Service	Goshen, Ind.
83777	Model Eng. and Mfg., Inc.	Huntington, Ind.	93780	Howard J. Smith, Inc.	Port Monmouth, N.J.	98405	Carac Corp.	Redwood City, Calif.	000HH	Rubbercraft Corp.	Torrance, Calif.
83821	Loyd Scruggs Co.	Festus, Mo.	93923	G. V. Contois	Livingston, N.J.	98731	General Mills	Minneapolis, Minn.	000II	Bratcher Corporation, Industrial Division	Monterey Park, Calif.
84177	Arco Electronics, Inc.	New York, N.Y.	93983	Insuline-Van Norman Ind., Inc., Electronic Division	Manchester, N.H.	98821	North Hills Electric Co.	Mineola, N.Y.	000KK	Amatol	New Rochelle, N.Y.
84295	A. J. Glechner Co., Inc.	San Francisco, Calif.	34144	Raytheon Mfg. Co., Industrial Components Div., Receiving Tube Operation	Quincy, Mass.	98925	Clevite Transistor Prod., Div. of Clevite Corp.	Waltham, Mass.	000LL	Avery Label	Monrovia, Calif.
84411	Good All Electric Mfg. Co.	Ogallala, Neb.	34144	Raytheon Mfg. Co., Industrial Components Div., Receiving Tube Operation	Quincy, Mass.	99378	International Electronic Research Corp.	Burbank, Calif.	000MM	Rubber Eng. & Development	Hayward, Calif.
84570	Sarkes Tarzian, Inc.	Blomington, Ind.	94145	Raytheon Mfg. Co., Semiconductor Div., California Street Plant	Newton, Mass.	99109	Columbia Technical Corp.	New York, N.Y.	000NN	A 'N' D Manufacturing Co.	San Jose 27, Calif.
85454	Boonton Molding Company	Boonton, N.J.	94148	Scientific Radio Products, Inc.	Loveland, Colo.	99313	Varian Associates	Palo Alto, Calif.	000PP	Atmos Electronics	Sun Valley, Calif.
85474	R. M. Bracamonte & Co.	San Francisco, Calif.	94154	Tung-Sol Electric, Inc.	Newark, N.J.	99515	Marshall Industries, Electron Products Division	Pasadena, Calif.	000QQ	Coultion	Oakland, Calif.
85660	Koled Kords, Inc.	New Haven, Conn.	94197	Curtiss-Wright Corp., Electronics Div.	East Paterson, N.J.	99707	Control Switch Division, Cetecos Co., of America	El Segundo, Calif.	000RR	Radio Industries	Des Plaines, Ill.
85911	Seamless Rubber Co.	Chicago, Ill.	94222	Southco Div. of S. Chester Corp.	Leslie, Pa.	99800	Defelean Electronics Corp.	East Aurora, N.Y.	000SS	Control of Elgin Watch Co.	Burbank, Calif.
86197	Clifton Precision Products	Clifton Heights, Pa.	94310	Tia Ohm Prod. Div. of Model Engineering and Mfg. Co.	Chicago, Ill.	99848	Wilco Corporation	Indianapolis, Ind.	000WW	California Eastern Lab.	Burlingame, Calif.
86579	Precision Rubber Products Corp.	Dayton, Ohio	94682	Worcester Pressed Aluminum Corp.	Worcester, Mass.	99934	Renbrandt, Inc.	Boston, Mass.	000XX	Methode Electronics, Inc.	Chicago 31, Ill.
86684	Radio Corp. of America, RCA	Harrison, N.J.	95023	Philbrick Researchers, Inc.	Boston, Mass.	99942	Hoffman Semiconductor Div. of Hoffman Electronics Corp.	Evanston, Ill.	000YY	S. K. Smith Co.	Los Angeles 45, Calif.
87216	Phico Corporation (Lansdale Division)	Lansdale, Pa.	95236	Allies Products Corp.	Miami, Fla.	99957	Technology Instrument Corp. of Calif.	Newbury Park, Calif.			
87473	Western Fibrous Glass Products Co.	San Francisco, Calif.									
87564	Van Waters & Rogers Inc.	Seattle, Wash.									
88140	Cutter-Hammer, Inc.	Lincoln, Ill.									

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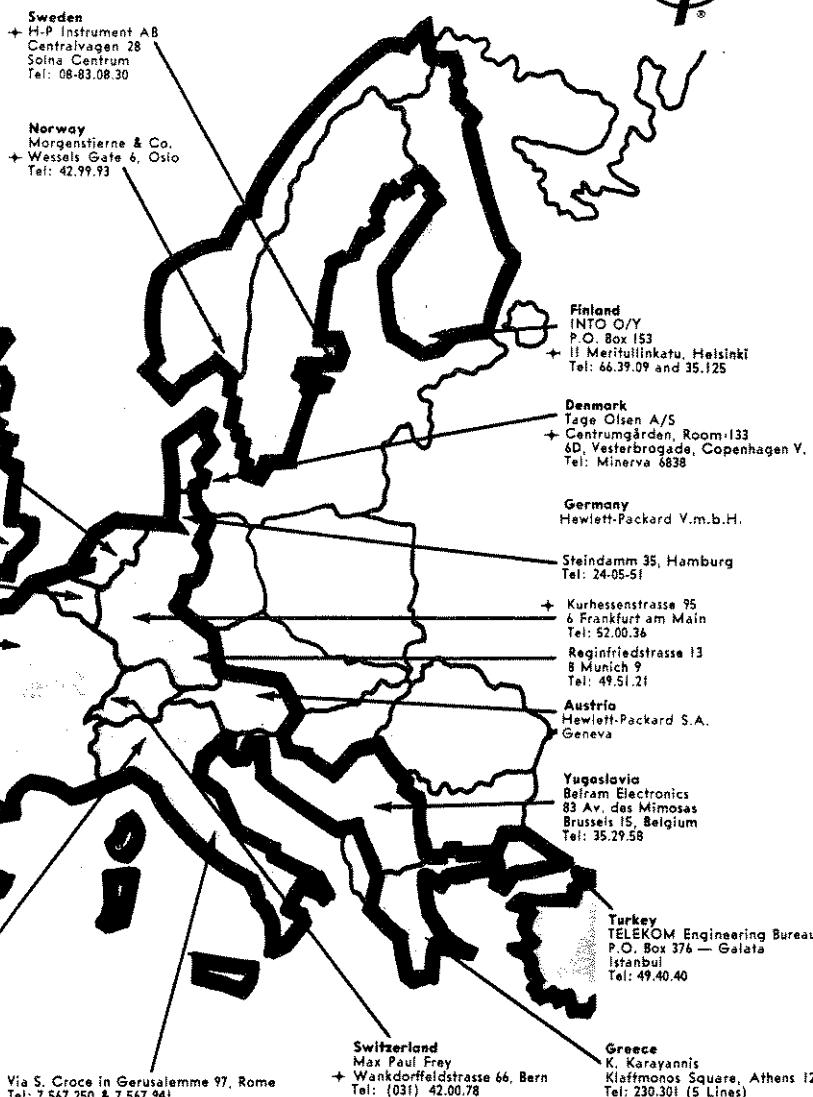
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Tel: 43850, 48111

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+ 16 Kremenevski St., Tel Aviv  
Tel: 35021 (3 lines)

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Onehunga S. E. S., Auckland  
Tel: 565-361

**Puerto Rico & Virgin Islands**  
San Juan Electronics, Inc.  
P.O. Box 5167  
Pta. de Tierra Sta., San Juan  
Tel: 722-3342, 724-4404

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Rosella House  
Buitengracht Street, Cape Town  
Tel: 3-3817

**Taiwan (Formosa)**  
Hwa Sheng Electronic Co., Ltd.  
21 Nanking West Road, Taipei  
Tel: 4-6076, 4-5936

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